Phase 1: Lincoln Street Subwatershed Nutrient Control Strategies

FINAL REPORT - JUNE 2017

Water Integration for Squamscott-Exeter (WISE) Integrated Plan



Prepared for: Town of Exeter, New Hampshire COUNDED 1638

Prepared by: Waterstone Engineering, PLLC

Funded by: NOAA Office for Coastal Management NH Coastal Program









Phase 1: Lincoln Street Subwatershed

Nutrient Control Strategies

FINAL REPORT

Project:

Water Integration for Squamscott-Exeter (WISE) Integrated Plan

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ACRONYMS

AOC	Administrative Order on Consent
BMP	Best Management Practice
CSO	Combined Sewer Overflows
CIP	Capital Improvement Plans
CWA	Clean Water Act
EPA	United States Environmental Protection Agency
GBNNPSS	Great Bay Nutrient Nonpoint Source Study
GI	Green Infrastructure
HRU	Hydrologic Response Unit
I/I	Inflow and Infiltration
IP	Integrated Planning
LID	Low Impact Development
MEP	Maximum Extent Practicable
MS4	Municipal Separate Storm Sewer System
NHDES	New Hampshire Department of Environmental Services
NLM	Nitrogen Load Model
NPDES	National Pollution Discharge Elimination System
NPS	Nonpoint source pollution
NRCS	Natural Resources Conservation Service
O&M	Operations and Maintenance
ORIWMP	Oyster River Integrated Watershed Management Plan
PREP	Piscataqua Region Estuaries Partnership
PTAPP	Pollution Tracking and Accounting Pilot Program
ROW	Right-of-way
SSO	Sanitary Sewer Overflow
SWMM	EPA Stormwater Management Model
TMDL	Total Maximum Daily Load
TN	Total Nitrgen
UNH	University of New Hampshire
WISE	Water Integration for the Squamscott-Exeter
WLA	Waste Load Allocation
WQRP	Water Quality Response Plan
WWTF	Wastewater Treatment Facility



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What is the Lincoln Street Subwatershed Nutrient Control Strategies Report?

This report presents information from the Lincoln Street Subwatershed Nutrient Control Strategies, Phase 1, Water Integration for Squamscott-Exeter (WISE) Integrated Plan. This project (conducted from 2016-2017) builds upon recommended activities detailed in the Plan which will help satisfy permit requirements for wastewater and stormwater management and increase climate resiliency for municipal drainage infrastructure.

This project provides a plan and design to support the 2017-2018 Lincoln Street Capital Improvement Plan for Utilities and Road Reconstruction. The capital project is based on a complete street approach that balances mobility and safety for all users while creating a healthier place – socially, environmentally, and for the local economy. A complete street approach combines the use of green infrastructure with attractive public spaces for the community and local businesses to help reduce nitrogen and flooding from stormwater runoff. This project conducted watershed planning and designs for green infrastructure strategies in the Town's largest subwatershed for use in future CIP, and grant program applications. The project uses recommendations from the 2015 Integrated Plan and involved priority sites with the highest pollutant load that discharge directly to the Squamscott-Exeter River.

The project has four primary objectives:

1. Increasing municipal capacity to identify and implement feasible and cost effective nutrient control strategies by beginning the implementation of the WISE Integrated Plan through the use of Plan recommendations and best management practice (BMP) sizing tools.



- 2. Reduce nitrogen load from a series of BMPs throughout the Lincoln Street subwatershed.
- 3. Increase climate resiliency by reducing flooding through installation of BMPs.
- 4. Development of construction-ready green infrastructure designs for inclusion in future capital improvement projects in Exeter's largest subwatershed.

Why Nutrient Control Planning?

New Hampshire coastal communities have experienced rising populations resulting in an increase in development in point source and non-point source nitrogen loads. As communities respond to new federal permit requirements for treating and discharging stormwater and wastewater, meeting regulatory requirements requires innovative ways to find effective and affordable means to meet water quality goals. Integrated Planning allows flexibility in permitting of wastewater and stormwater controls to plan for the most cost-effective measures first while still meeting regulatory standards that protect public health and water quality. It encourages the use of green infrastructure which manages stormwater as a resource, and supports other economic and quality of life benefits. Integrated planning is being shown to have great cost-efficiencies through the comprehensive management of wastewater, stormwater and nonpoint sources.

Major Findings

- Four priority locations were identified as feasible retrofits which include 14 individual stormwater best management practices (BMPs).
- Small BMPs designed to treat the first flush provide the greatest cost-effective nitrogen controls with 13 BMPs sized to treat 0.25-0.5" water quality volume.
- Implementation of these BMPs is expected to reduce nitrogen loading by 300 pounds per year and total runoff volume by 24 million gallons per year.
- The total cost for the 14 BMPs is estimated at \$309,800 at an average unit cost of \$1,040 per pound of nitrogen.

Project Team

The project team included Paul Vlasich, Town Engineer, Jennifer Mates, Assistant Town Engineer, Jay Perkins, Road Agent, Daniel Lewis, Engineering Technician, Jennifer Perry, Public Works Director from the Town of Exeter, Robert Roseen, Project Director, Jake Sahl, Modeler and Analyst from Waterstone Engineering, Sally Soule, Grant Manager, Steve Couture, Supervisor, of the New Hampshire Coastal Program.

Funding was provided by the New Hampshire Coastal Program for a project titled *Phase 1: Lincoln Street* Subwatershed Nutrient Control Strategies, Water Integration for Squamscott-Exeter (WISE) Integrated *Plan.*

1. INTRODUCTION



This project summary presents information from the Water Integration for Squamscott-Exeter (WISE) Integrated Plan Phase 1: Lincoln Street Subwatershed Nutrient Control Strategies by Waterstone Engineering. The project builds upon recommended activities detailed in the Plan which will satisfy permit requirements for wastewater and stormwater.

The study area is Exeter's largest watershed (S10¹) totaling 179 acres and comprised of 2 subwatersheds, the upper watershed area to the west (S10 West), and the lower area to the east of the railroad tracks (S10 East) which encompasses Lincoln Street. These areas drain underneath Phillips Exeter Academy to a known area of flooding concern along Tan Lane, the location of which makes upsizing sewer infrastructure very difficult. Management of upstream runoff will reduce flood vulnerability and provide water quality treatment in a more cost-effective manner than simply upgrading pipe size and capacity. Previous studies² used a drainage infrastructure model to identify several areas of concern within the watershed based on the likelihood of flooding. The flood risk at these locations (shown in Figure 1) has been confirmed by town staff. Using geospatial data for stormsewer lines, manholes, catch basins, and topography, drainage infrastructure components were categorized based on their watershed area. This allowed the project team to identify several sites where BMP installations would have large drainage areas and thus a significant potential to reduce flooding and improve water quality within the watershed.

This project identified locations and calculated the potential benefits from BMPs for nutrient management and climate resiliency. This report identifies locations of potential BMPs and presents estimates of the nitrogen load and storm volume reduction using BMP performance curves³. A suite of 14 priority BMPs were modeled for flood reduction potential and costing and 95% concept designs were completed for each.

¹ Drainage Area Map Package, Town of Exeter, December 29, 2014

² Climate Adaptation for Exeter (CAPE) Project, 2016

³ Water Integration for Squamscott Exeter (WISE, 2015), Draft Integrated Plan

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2. BACKGROUND



Like many coastal regions, population growth and development in Exeter has contributed to an increase in impervious cover and has led to increased pollutant loads and stormwater runoff. As more impervious surface is added, flooding risks are elevated and water quality is impacted. Recent documented changes in climate have resulted in higher-intensity precipitation events, increased rainfall depth, and greater variations in storm duration and frequency which increase these risks and impacts.

In 2009, NHDES concluded that many sub-estuaries in the Great Bay Estuary were impaired by nitrogen, and the Great Bay was placed on the Clean Water Act (CWA) Sec. 303(d) list of impaired and threatened waters (NHDES, 2009). New and revised discharge permits in the watershed are now subject to additional nitrogen requirements including the National Pollutant Discharge Elimination System (NPDES) permits for wastewater treatment facilities, and Municipal Separate Storm Sewer Discharge (MS4) permits for stormwater. In 2012 EPA issued a new NPDES wastewater discharge permit to the Town of Exeter with a total nitrogen (TN) effluent limit of 3 mg/l. The Town subsequently negotiated an Administrative Order of Consent (AOC) with the EPA that allows a staged approach to TN reduction, allowing 5 years to construct a facility to treat nitrogen to meet a limit of 8 mg/l TN, followed by continued upgrades and reductions in TN. The AOC requires a Total Nitrogen Nonpoint and Point Source Stormwater Control Plan by September 30, 2018. The plan must include a schedule for implementing specific nitrogen control measures. In addition, the new 2017 NH Small MS4, which becomes effective in 2018, includes significant new elements such as a focus on illicit discharge detection and elimination, and nutrient management through BMP retrofits. The town approved funding for a \$49.9 million new wastewater plant in March 2017 through the NH Clean Water State Revolving Loan Fund. Construction began in June 2017 and is expected to be completed in 2018.



Figure 1: Areas of interest for BMP Retrofit

3. STORMWATER MANAGEMENT



In March 2015, the Water Integration for Squamscott-Exeter (WISE) project completed an Integrated Planning framework for three coastal communities including Exeter, Stratham, and Newfields to provide recommendations for affordably managing permits for wastewater and stormwater. A watershed level load model was developed to determine the nitrogen load to the Squamscott-Exeter estuary. The results represent a baseline assessment to quantify the economic and performance advantages of integration of water resource planning both at the municipal and inter-municipal level. This project seeks to build upon the WISE analysis to identify specific green infrastructure (GI) and low impact development (LID) practices that can be installed in Exeter to manage stormwater, reduce nutrient loads, and increase resiliency.

The new 2017 MS4 permit requires management of existing stormwater runoff in impaired watersheds. While new development is required to manage stormwater on-site, existing developments were constructed before stormwater management was required and modern criteria established. Retrofits include new installations or upgrades to existing best management practices (BMPs) in developed areas draining to impaired waters and their tributaries.

BMPs for stormwater management and nitrogen controls include both structural and non-structural practices to reduce runoff volume from stormwater sources such as impervious surfaces (rooftops and parking lots), residential areas, commercial/industrial/institutional properties, roads, outdoor recreational spaces (i.e., parks), agricultural areas, and managed turf (i.e., golf courses, lawn). Common BMPs for nutrient controls include biofiltration (bioretention, raingardens, tree planters), gravel wetlands, infiltration practices (dry wells, and subsurface infiltration), and porous pavements. The Plan lists a range of BMPs that were reviewed and vetted by the towns with respect to land use and practicality. A wealth of BMP sources exists in the literature and locally at the UNH Stormwater Center. A list of practices can be found in the New Hampshire Stormwater Manual on the <u>NHDES website</u>.

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4. WATERSHED OVERVIEW



a. Watershed Status and Regulatory Framework

EPA is required to develop criteria (numeric or narrative) based on a determination that there exists a reasonable potential to cause or contribute to an impairment⁴. This determination is based on 'the best available science' at the time, which acknowledges that although our understanding of an ecosystem is necessarily incomplete, further delay in corrective measures will clearly contribute to increasing degradation. Permits may be issued to comply with numeric or narrative criteria. In 2009 NHDES developed draft numeric nutrient criteria for the protection of eelgrass and low dissolved oxygen conditions. In the absence of final numeric criteria EPA asserts the obligation and authority to issue effluent limitations based on a narrative criteria and in 2012 EPA issued final WWTF discharge permits in Newmarket and Exeter based on a narrative TN nutrient criteria and a reasonable potential analysis. A 2014 Peer Review was critical of the draft numeric criteria after which the criteria were dropped as part of a 2014 settlement agreement between NHDES and the Municipal Coalition⁵. The standard upon which the Peer Review was tasked to review the draft numeric criteria was in part…" whether the available data support the conclusion that excess nitrogen was the primary factor that caused (1) the decline of eelgrass populations…"⁶ This determination as the "primary factor that caused" is a higher standard than a "reasonable potential to cause or contribute". In 2012 the Environmental Appeals Board and, in 2013 the Supreme Court, upheld the basis

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⁴ Pg. 143, Section 5. Reasonable Potential Analysis and Effluent Limit Derivation, EPA. (2012). "Authorization to Discharge Under the National Pollutant Discharge Elimination System, The Town of Exeter, New Hampshire, Squamscott River." NPDES Permit No. NH0100871, Office of Ecosystem Protection, U.S. Environmental Protection Agency, Region I, Boston, Massachusetts.

⁵ April 2014, Settlement Agreement between the Great Bay Municipal Coalition (Portsmouth, Dover, Rochester, NH) and the State of New Hampshire.

⁶ Pg 46, section b) from the "Joint Report of Peer Review Panel-Great Bay Estuary", February 13, 2014 Victor J. Bierman, Robert J. Diaz, W. Judson Kenworthy, Kenneth H. Reckhow.

for this finding by EPA in determining effluent limitations⁷. In 2016, the Piscataqua Region Estuaries Partnership reconvened the technical advisory committee to review indicator trends and status. In so doing they convened a panel of experts including Jud Kenworthy, the eelgrass expert from the Peer Review, to review eelgrass stressors. They affirmed the position that nitrogen was indeed a major factor and has a reasonable potential to cause or contribute to the environmental problem.

b. Watershed Land Use and Growth Trends

Exeter has experienced substantial growth during the past 50 years. Understanding and mitigating impacts due to population increase, changes in land use and cover, and imperviousness are an essential element of effective management strategies. Since 1960 Exeter has experienced 98% population growth and a 20 year increase in impervious cover of 108% (Figure 2).



Figure 2 - Population and Impervious Cover changes in the Towns of Exeter, Newfields and Stratham

The study area is comprised of 2 distinct watersheds in terms of drainage infrastructure, the upper watershed area to the west (S10 West), and the lower area to the east of the railroad tracks (S10 East) as displayed in Figure 2. The total watershed is 41% impervious cover, 179 acres, and contributes an estimated 1,265 lbs of nitrogen annually, as shown in Table 1. The watershed land use is predominantly commercial, residential, and roadways. The upper watershed is 57 acres and contributes an estimated 390 lbs of nitrogen annually (Appendix A). The lower watershed, including Lincoln Street, is the larger of the two at 122 acres and contributes an estimated 876 lbs of nitrogen annually (Appendix A). These areas all drain into a 27" storm drain underneath Phillips Exeter Academy to a known area of flooding concern along Tan Lane, the location of which makes upsizing very difficult. Management of upstream runoff will reduce flood vulnerability and provide water quality treatment in a more cost-effective manner than simply upgrading pipe size and capacity. The growth trends in the area will require planning efforts and administrative tools to protect water quality. Communities are all in need of cost-effective strategies from meeting permit requirements to assist in balancing the range of competing municipal demands.

⁷ (2012). "Upper Blackstone Water Pollution Dist. v. EPA." F. 3d, Court of Appeals, 1st Circuit, 9.

Land Use Type	Hydrologic Soil Group*	Area (acres)	Annual Nitrogen Export (Ibs)**
Agriculturo	А	0.04	0.02
Agriculture	C/D	0.47	1.51
Commercial Services and	А	6.44	3.42
Institutional	C/D	15.48	41.48
	IMP	30.72	424.48
	А	3.62	1.01
Forest	C/D	2.69	3.88
	IMP	0.02	0.27
Industrial and Commercial Complexes	C/D	0.00	0.01
	IMP	0.77	10.64
Outdoor and Other Urban and Built	А	1.83	2.00
	C/D	6.15	34.07
	IMP	0.48	6.62
	А	20.41	10.82
Residential	C/D	47.59	127.53
	IMP	26.26	413.04
	A	0.09	0.02
Transitional	C/D	0.23	0.31
	IMP	0.19	2.68
Transportation Communications and	А	0.16	0.04
Italisportation, communications, and	C/D	0.14	0.17
	IMP	16.17	182.87
Totals		179	1,265

 Table 1: Lincoln Street Total Watershed Characteristics

* Hydrologic soil group derived from landform. Watershed area was divided into 3 slope classes, 0-3%, 3-8%, and 8-15%. Dominant soil type for each slope class was assumed for entire slope class. Scitico silt loam for 0-3% slopes, Charlton fine sandy loam for others. **Based on WISE, 2015 PLERs

c. Environmental Impacts from Growth

Monitoring and research conducted by various university, local, state and federal programs and projects have documented stresses in the Great Bay system. Prominent drivers of change include watershed modification and development resulting in increased impervious cover; increased nutrient and pollutant loading from a rapidly growing coastal population; and ecosystem instability and loss of diversity caused by invasive species, habitat destruction, disease, and others. Each stress drives additional physical, chemical, and biological pressures on the Great Bay system that effect the environmental, lifestyle, and economic benefits valued by local communities. Environmental indicators used by the National Estuaries Program to identify and track ecosystem health clearly illustrate an ecosystem in trouble. In the most recent State of Our Estuaries 2013 report (PREP, 2013), 12 of 16 indicators showed a declining or cautionary condition. Impervious cover, an indicator of development, shows a long-term increasing trend which is related to condition indicators including nutrient concentration, eelgrass, dissolved oxygen, and macroalgae that show either no improvement or continued quality decline.

d. NPDES Wastewater Permit and Administrative Order of Consent

EPA Region 1 issues individual facility-specific permits for the discharge of treated domestic and industrial wastewater in the State of New Hampshire. Under these individual permits, the discharges will be limited and monitored by the permittee. Of the three WISE watershed communities, the Towns of Exeter and Newfields operate and discharge treated domestic wastewater.

In 2012 after several years of study and negotiations, EPA issued a new NPDES discharge permit to the Town of Exeter with a total nitrogen (TN) effluent limit of 3 mg/l. The Town subsequently negotiated an Administrative Order on Consent (AOC) with the EPA that allows a staged approach to TN reduction which allows 5 years to construct a facility which will treat nitrogen to meet a limit of 8 mg/l TN, followed by continued upgrades and reductions in TN. The AOC requires tracking and monitoring to ensure that load reductions goals and ecosystem response are on target.

e. Municipal Separate Storm Sewer System (MS4)

Under the MS4 program, towns with urbanized areas as defined by the US Census are required to obtain permit coverage for their stormwater discharges. Exeter is subject to the requirements of EPA's 2017 NH Small MS4 General Permit for stormwater discharges. EPA released a final permit in 2017 which contained new provisions for the 6 Minimum Measures (MM):

- 1) Public Education and Outreach
- 2) Public Participation/Involvement
- 3) Illicit Discharge Detection and Elimination
- 4) Construction Site Runoff Control
- 5) Post-Construction Runoff Control
- 6) Pollution Prevention/Good Housekeeping

The draft permit also includes new requirements to develop Water Quality Response Plans (WQRPs) for stormwater outfalls that discharge to impaired water bodies. The WQRPs will assess all significant discharges to determine if they could contribute to the waterbody impairment and identify BMPs and a schedule for implementation to address the impairments.

f. EPA Integrated Planning Framework and Watershed Based Planning

The June 2012 EPA memorandum, "Integrated Municipal Stormwater and Wastewater Planning Approach Framework" provides guidance for EPA, States and local governments to develop and implement effective integrated plans that satisfy the CWA. The framework outlines the overarching principles and essential elements of a successful integrated plan which includes:

• Maintaining existing regulatory standards that protect public health and water quality.

- Allowing a municipality to balance CWA requirements in a manner that addresses the most pressing public health and environmental protection issues first.
- The responsibility to develop an integrated plan rests on the municipality that chooses to pursue the approach. EPA and/or the State will determine appropriate actions, which may include developing requirements and schedules in enforceable documents.
- Innovative technologies, including green infrastructure, are important tools that can generate many benefits, and may be fundamental aspects of municipalities' plans for integrated solutions.

The elements in the WISE plan are consistent with guidance issued by EPA to support integrated permit planning, as well as the Agency's nine-element watershed plans.

g. Municipal Regulations

For the Integrated Plan to be effective, future regulations will need to be adopted by Exeter that include: 1) provisions for new and redevelopment projects to require nitrogen controls, and 2) a means for tracking changes in significant land use activities that will impact the nitrogen load to surface waters. Exeter is participating in PTAPP (the Pollution Tracking and Accounting Pilot Program) which in June 2017 developed a draft uniform approach using a web based application that can be used by communities for MS4 and AOC tracking and accounting.

The March 2015 Piscataqua Region Environmental Planning Assessment report (PREPA) recommends Exeter adopt fertilizer application buffers for all surface waters, increase the no vegetation disturbance to 100' on tidal wetlands, and adopt the Southeast Watershed Alliance Model Stormwater Management Regulations.

h. Southeast Watershed Alliance Model Stormwater Management Regulations

The Southeast Watershed Alliance developed model stormwater standards in 2012, and revised in 2017, to provide minimum, consistent, and effective model stormwater management standards for communities in the Great Bay. These standards are intended to address some of the requirements for communities subject to the MS4 permit. The model standards include 7 critical core elements: Applicability Standards, Minimum Thresholds for Applicability, Best Management Practices, Applicability for Redevelopment, Stormwater Management Plan Approval and Recordation, Maintenance Criteria, Inspection of Infrastructure.

i. Impaired Waters

The Clean Water Act requires each state to submit a list of impaired waters to the U.S. Environmental Protection Agency every two years. Listing of impaired waters (303d list) includes surface waters that:

- Are impaired or threatened by a pollutant or pollutant(s),
- Are not expected to meet water quality standards within a reasonable time even after application of best available technology standards for point sources or best management practices for nonpoint sources and,
- Require development and implementation of a comprehensive water quality study (i.e., called a Total Maximum Daily Load or TMDL study) that is designed to meet water quality standards.

As of the final 2008 listing, the impaired waters within the Town of Exeter include: Dudley Brook; Norris Brook; Little River; Squamscott River; Wheelwright Creek- Parkman Brook; Exeter River; Colcord Pond; and Little River – Scamen Brook. Under the MS4, Exeter is required to manage the drainage area and infrastructure to receiving waters and implement controls to reduce sources of impairments.

5. SITE SELECTION AND BMP FEASIBILITY



A field assessment was performed at each of the seven locations shown in Figure 1 to determine the soil classification and feasibility for BMP retrofit. Soil coring was conducted on November 28th, and December 6th-7th, 2016. Soils were sampled at six of the seven sites. The seventh site, located behind Lincoln Street Elementary School was too gravelly to be cored and the soil type of that site was assumed to be the same as that of sites 3 and 4 given the geographic proximity and similarity in landform characteristics (e.g. slope).

Soil cores indicated that 5 of the 6 sites are fine sandy loams with lower horizons as fine sands. The dominant soil type (found in sites 1, 2, 3, 4, 5, and also assumed to be found 7) is a 62B: Charlton Fine Sandy Loam⁸. The soil samples from site 6 were more characteristic of a 33A: Scitico Silt Loam⁸ with largely clay and silt features below the upper horizon. Appendix B describes each site's soil type, hydrologic soil group, published saturated hydraulic conductivity, and also contains a detailed field soil log.

Based on the physical characteristics of each site, a few suitable BMP types were identified. Subsurface infiltration systems with pre-treatment are applicable in parks or open space locations that have enough available area to house large storage chambers intended to divert flow from within the storm drain network and thereby treat large upstream drainage areas. ROW retrofits are applicable within the roadside right-of-way (ROW) and designed to treat surface runoff from roads and surrounding areas through connection into the existing drainage network. These systems can include tree planters, bioretention, and/or infiltration for stormwater treatment.

⁸ NRCS Soil Survey designation number and description

6. BEST MANAGEMENT PRACTICE RETROFIT OPPORTUNITIES



For each of the seven locations discussed above, a feasibility analysis was performed based on location, upstream drainage area, and soil characteristics to determine its potential for a BMP retrofit. The location of BMPs focused on the feasibility of utilizing publicly controlled areas such as right-of-ways, parks, and open spaces.

Figure 1 depicts the seven sites within the watershed that were chosen for assessment. Ultimately, a suite of 14 BMPs were chosen for installation at sites, 1, 2, 3, and 5. Table 2 presents the BMP and upstream drainage area characteristics for these 14 BMPs.

a. Example Best Management Practices for Nutrient Control and Climate Resiliency

There are several best management practices that can be used in municipal, commercial, industrial, and residential areas to manage runoff from roof tops, impervious surfaces, and pervious surfaces. These include dry wells, subsurface infiltration systems, gravel wetlands, porous pavements, biofiltration, and high efficiency bioretention.

Figure 3 illustrates a tree planter installed as part of road reconstruction and sewer improvements. The tree planter combines a tree well and catchbasin with an engineered soil that provides a growing medium and water quality filter. The planter was designed with an eye towards low maintenance, especially during the winter. Tree planters like these can be cleared easily by snow plow and the



Figure 3: Tree Planter Combined with Catch Basin

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sediment and debris removal process is limited to a deep sump and cleaning by vactor truck. With the tree planter grate the sidewalk area is usable for pedestrian travel.

Tree planters, bioretention, and other forms of infiltration or biofiltration can be combined with streetscapes for added functionality. Figure 4 shows a bioretention system located in a parking lot that could be applied in road right-of-way.



Figure 5 - Streetscape with Street Trees Adaptable for Stormwater Management



Figure 4: Parking Lot Bioretention

Figure 5 is an example of a streetscape and tree planter that could easily be combined for stormwater management. The street scape has a combination of pedestrian considerations, space for local business to use the sidewalks, and park benches, all of which could allow for use of some type of planter or infiltration system below ground.

Figure 6 shows a large scale subsurface infiltration system combined with an isolator row for pretreatment. The isolator row is a wrapped chamber that prevents clogging of the stone bed. A subsurface infiltration system such as this combined with a pretreatment design could be used effectively for flood control and nutrient reduction.



Figure 6: Subsurface Infiltration with Stone Reservoir and Isolator Row Pretreatment Chamber

Location	BMP #	ВМР Туре	Soil Type	Drainage Area (acres)	Annual TN Load (lbs)	System Size
	1	Subsurface Infiltration	А	12.88	90.1	1/2" WQV
WINTER STREET	2*	Subsurface Infiltration	А	24.56	157.6	1/2" WQV
	3.1	Tree Planter	А	0.20	2.5	1/2" WQV
	3.2	Tree Planter	А	0.13	1.7	1/2" WQV
	3.3	Tree Planter	А	0.27	3.4	1/2" WQV
	3.4	Tree Planter	А	0.22	2.9	1/2" WQV
LINCOLN STREET NORTH	3.5	ROW Infiltration- Grassed	А	0.24	2.4	1/2" WQV
	3.6	ROW Infiltration- Grassed	А	0.78	7.2	1/2" WQV
	3.8	ROW Infiltration- Grassed	А	1.20	9.1	1/2" WQV
	3.9	ROW Infiltration- Grassed	А	0.70	5.6	1/2" WQV
	3.22	ROW Infiltration- Grassed	А	0.20	1.3	1/2" WQV
	3.20	ROW Infiltration- Grassed	А	1.60	13.9	1/2" WQV
LINCOLN STREET SOUTH	3.21	ROW Infiltration- Grassed	А	0.24	1.4	1/2" WQV
FRONT STREET	5	Subsurface Infiltration	А	20.29	138.3	1/4" WQV
Totals	-	-	-	63.5	437.5	-

Table 2 - BMP and Drainage Area Characteristics

* Drainage area and Annual TN Load estimates exclude area and load managed by BMP 1

b. BMP 1: Subsurface Infiltration at the Intersection of Winter and Front Street

BMP 1 was chosen for full 95% design and costing. It is located in a public playground at the intersection of Winter Street and Front Street (Figure 7). Soils test pits within this site identified fine sandy loams that are highly suitable for infiltration as they fall in hydrologic soil group A. The project team assessed the impacts of installing a subsurface infiltration treatment system to manage the 13-acre upstream drainage area.



Figure 7: BMP 1 Subsurface Infiltration at the Intersection of Winter and Front Street

Subsurface infiltration systems of several sizes were modeled to compare the costs of construction against the nutrient loading and flood reduction benefits. The three sizes that were considered were a ¹/₄" water quality volume system (big enough to fully capture the 1st ¹/₄" of runoff from the upstream drainage area), a ¹/₂" WQV system, and a 'flood sized' system big enough to capture runoff from an event slightly smaller than the 2-year storm (this was the maximum potential size based on the proposed site).

Ultimately, it was decided that the ¹/₂" WQV system would provide the most benefit relative to the associated costs. This BMP is expected to manage 68.2 lbs of nitrogen annually, leading to a 76% load reduction from the upstream drainage area at a total cost of \$45,900. It will also reduce flooding extent and duration downstream during large storm events, including along Railroad Avenue. Figure 8 shows the 95% engineering design for BMP 1.



Figure 8: Engineering Detail for Winter Street Subsurface Infiltration BMP 1

c. BMP 2: Subsurface Infiltration at Columbus Ave., Winter St., Railroad Ave. Intersection BMP 2 was chosen for full 95% design and costing. It is located in a small park at the intersection of Columbus Avenue, Winter Street, and Railroad Avenue (Figure 9). The project team assessed the impacts of installing a subsurface infiltration system to manage the 25-acre upstream drainage area. Soil test pits within this site found fine sandy loams highly suitable for infiltration as they fall in hydrologic soil group A. Some reconfiguration of the drainage infrastructure would be required to divert flows and is described in Appendix A.



Figure 9: BMP 2 Subsurface Infiltration Site at the Intersection of Columbus Ave., Winter St., and Railroad Ave.

Subsurface infiltration systems of several sizes were modeled to compare the costs of construction against the nutrient loading and flood reduction benefits. The three sizes that were considered were a $\frac{1}{4}$ " water quality volume system (big enough to fully capture the 1st $\frac{1}{4}$ " of runoff from the upstream drainage area), a $\frac{1}{2}$ " WQV system, and a 'flood sized' system of the maximum potential size based on the proposed site.

Ultimately, it was decided that the $\frac{1}{2}$ " WQV system would provide the most benefit relative to the associated costs. This BMP is expected to manage 120.2 lbs of nitrogen annually, leading to a 76% load reduction from the upstream drainage area at a total cost of \$79,000. It will also reduce flooding extent and duration downstream during large storm events, including along Railroad Avenue. Figure 10 shows the 95% engineering design for BMP 2.



Figure 10: Engineering Detail for Railroad Avenue Subsurface Infiltration BMP 2

d. BMP 3: ROW Infiltration on Lincoln Street

BMP 3 was chosen for full 95% design and costing. It consists of numerous (11) small systems located in the public right-of-way on Lincoln Street. These BMPs will be a mix of tree planters and right-of-way infiltration systems located in the public right-of-way. These BMPs would manage surface and road runoff from 5.8 acres (Figure 11). Soils within this site are fine sandy loams and are highly suitable for infiltration as they fall in hydrologic soil group A.



Figure 11: BMP 3 ROW Infiltration Site on Lincoln Street

ROW infiltration systems of several sizes were modeled to compare the costs of construction against the nutrient loading and flood reduction benefits. The three sizes that were considered were a ¹/₄" water quality volume system (big enough to fully capture the 1st ¹/₄" of runoff from the upstream drainage area), a ¹/₂" WQV system, and a 'flood sized' system of the maximum potential size based on the proposed site.

Ultimately, it was decided that the ¹/₂" WQV systems would provide the most benefit relative to the associated costs. These BMPs are expected to manage 39.6 lbs of nitrogen annually, leading to a 77% load reduction from the upstream drainage area at a total cost of \$139,700. It will also reduce flooding extent and duration downstream during large storm events. Figure 12 and Figure 13 show the 95% engineering designs for BMPs 3.1-3.22.



Figure 12: Engineering Detail for Lincoln Street North, Tree Planter BMPs 3.1 -3.4

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Figure 13: Engineering Detail for Lincoln Street South Right-of-Way Infiltration BMPs 3.5, 3.6, 3.8, 3.9, 3.20, 3.21, 3.22

e. BMP 4: Subsurface Infiltration at Lincoln Street Elementary School Parking Lot

BMP 4 was not chosen for design and costing under this project but will be pursued in a future Phase II analysis. The proposed site for BMP 4 is located behind the Lincoln Street Elementary School parking lot (Figure 14). The entire upstream drainage area is 76 acres, which would be reduced to 33 acres with the installation of BMPs 1, 2, and 3. Soils within this site are fine sandy loams and are suitable for infiltration however there is a shallow depth to groundwater that would need to be further evaluated. Given the size of the usable area, it may be feasible to install a subsurface infiltration treatment system within this site.



Figure 14: BMP 4 Subsurface Infiltration Site at the Lincoln Street Elementary School Parking Lot

f. BMP 5: ROW Infiltration/Filtration on Front Street

BMP 5 was chosen for full 95% design and costing. It is located in the public right-of-way on Front Street in front of Philips Exeter Academy (Figure 15). Soils within this site are fine sandy loams and are highly suitable for infiltration. The project team assessed the impacts of installing a subsurface infiltration treatment system to manage the 20-acre upstream drainage area.



Figure 15: BMP 5 ROW Infiltration/Filtration Site on Front Street

Subsurface infiltration systems of several sizes were modeled to compare the costs of construction against the nutrient loading and flood reduction benefits. The three sizes that were considered were a $\frac{1}{4}$ " water quality volume system (big enough to fully capture the 1^{st} $\frac{1}{4}$ " of runoff from the upstream drainage area), a $\frac{1}{2}$ " WQV system, and a 'flood sized' system of the maximum potential size based on the proposed site.

Ultimately, it was decided that the ¼" WQV system would provide the most benefit relative to the associated costs. This BMP is expected to manage 71.7 lbs of nitrogen annually, leading to a 52% load reduction from the upstream drainage area at a total cost of \$45,200. It will also reduce flooding extent and duration downstream during large storm events. Figure 16 shows the 95% engineering designs for BMP 5.



Figure 16: Engineering Detail for Front Street Subsurface Infiltration BMP 5

g. BMP 6: ROW Infiltration/Filtration on Washington Street

BMP 6 was not chosen for design and costing under this project but may be pursued in future phases. The proposed site for BMP 6 is located in the public right- of-way on Washington Street and could manage 1.7 acres of runoff (Figure 17). Soils within this site are silty clays and are not ideal for infiltration as they fall in hydrologic soil group C/D. This site is suitable for ROW infiltration, tree planters, or bioretention. Ultimately, it was decided that this is a low-priority BMP compared to the others considered during this effort. It could be re-examined at a later date in order to reduce the demands on downstream BMPs (primarily 1 and 2).



Figure 17: BMP 6 ROW Infiltration/Filtration Site on Washington Street

h. BMP 7: Subsurface Infiltration in the Lincoln Street Elementary School Fields

BMP 7 was not chosen for design and costing under this project but will be pursued in future a Phase II analysis. The proposed site for BMP 7 is located behind the Lincoln Street Elementary School in a large grassed area (Figure 18). Test pits were not conducted at this site but given the proximity and similarity in landform (e.g. slope), soil conditions are assumed to be similar to sites 3 and 4. Given the size of the usable area, it could be feasible to install a large subsurface infiltration treatment system within this site with 29 acres of upstream drainage area.



Figure 18: BMP 7 Subsurface Infiltration at Lincoln Street Elementary School

i. BMP Optimization and Lowest Cost Option

One of the core elements of integrated planning is the allowance that a permittee can take credit for actions associated with one permit (i.e., wastewater) while simultaneously receiving credit under another (i.e., MS4). For example, installation of green infrastructure (i.e., biofiltration to treat road runoff, or drywells to treat runoff from roof tops) for non-point source management under the WWTF permit would also satisfy requirements for Post Construction Stormwater Management (Minimum Measure 5) in the 2017 NH Small MS4 permit. This has the potential to be more economical than traditional permitting because it satisfies elements of both the MS4 and wastewater permits and it helps manage the uncertainty of environmental response.

Integrated planning also allows for flexibility as to when and what runoff management measures are implemented so long as the goal is the protection of public health and water quality. This approach allows for the use of various sizes (i.e., capture depths) of BMPs to allow for a greater number of smaller systems in replace of fewer systems designed to treat larger volumes.

An optimization model was developed as part of WISE which selects the most cost effective management measures for a range of runoff reduction levels. The optimization model runs iteratively, changing the target volume reduction with each iteration. It evaluates the runoff control strategies based upon user defined constraints including available land for implementation, volume reduction capability based on capture depth of the BMP, and cost to implement the strategy. This is first applied at the system level to develop a series of BMP performance curves. It is next applied at the land use scale to identify the most cost effective options for each particular land use. The optimization is then conducted at the watershed scale for the range of available runoff control measures, given the range of land uses within the wastershed. Appendix E presents BMP optimization and costing examples.
7. WATERSHED ANALYSIS



This section provides a summary of the methodology behind the water quality and hydrologic and hydraulic stormwater runoff model ("Model") for the Town of Exeter storm drainage infrastructure, initially developed as part of the Climate Adaptation Plan for Exeter (CAPE) project and WISE pollutant load model, and updated as part of this effort. A more in-depth description can be found in Appendix D of this document. The Model was created using the US Environmental Protection Agency (USEPA) Storm Water Management Model (SWMM) modeling platform to evaluate water quality and flooding potential of the stormwater infrastructure network under varying storm depths and future buildout conditions. The Model was used to investigate the flooding and surcharging of town storm drainage infrastructure during the 10-yr, 24-hr design storm (event depth of 4.72")⁹. The Model was created for planning purposes and includes some simplifying assumptions; it is not intended to provide design parameters for stormwater infrastructure installation and/or replacement. The preliminary stormwater infrastructure designs prepared for the Town of Exeter included independent detailed hydraulic/hydrologic analysis. Detailed information is provided in Appendix D: Watershed Modeling Methodology.

BMP designs and associated modeling calculations were performed with the HydroCAD (v 9.1) software package. Hydrographs are prepared for each element of the watershed and routed through the dynamic-storage-indication method to produce various time-based results. Runoff results from 0.25" and 0.5" WQV 24-hour design storms were used to develop appropriately sized treatment systems. These designs were then translated to the SWMM model to determine the larger watershed impacts.

Each of the proposed BMPs 1, 2, and 5 requires the addition of a weir in the existing drainage network in order to re-direct flow to the infiltration system. One major concern is to ensure that sufficient velocity exists for scouring sediment within the pipe network and to avoid added maintenance. A hydraulic analysis was conducted to evaluate pipe flow velocities upstream of BMPs 1, 2, and 5 both with and without the proposed weirs. The analysis showed that sufficient flow velocities will be maintained even with the addition of the weirs. The velocities drop near the weir for the water quality design of 0.25-0.5"

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⁹ Methodology and results are summarized in the memorandum prepared by Geosyntec Consultants, dated 21 October 2016, entitled "Storm Sewer Infrastructure Model Evaluation; 10-yr Design Storm Analysis; Exeter, New Hampshire"

and for greater storms the velocity remains high and pipe scour will occur insuring no issues with sedimentation. A table showing detailed modeling results for this analysis is provided in Appendix A.

8. BMP PERFORMANCE AND POLLUTANT LOAD REDUCTION



For each location and proposed BMP a pollutant loading analysis was performed in order to quantify the potential to reduce total nitrogen loads from the Lincoln Street watershed. Nitrogen removal performance was based on values derived as part of the WISE (2015) study, using pollutant load export rates (PLERs), BMP types, drainage areas, land uses, and soil types. Results were compiled for the final recommended BMPs (1, 2, 3, and 5) and are presented in Table 3.

The greatest potential nitrogen load reductions are expected from BMPs 1, 2, and 5, due to the fact that the drainage areas for each of these BMPs are quite large. All of the BMPs, with the exception of BMP 5, are expected to control roughly $\frac{3}{4}$ of the total nitrogen load from their respective drainage area. The reason that the portion of total load reduction associated with BMP 5 is much lower than the other systems is because this system was only sized to manage the $\frac{1}{4}$ " water quality volume due to space constraints at the proposed site.

The total annual nitrogen load from the entire Lincoln Street watershed is 1,265 pound. Installation of BMPs 1, 2, 3, and 5 is expected to reduce this load to 300 pounds annually, a 34% reduction.

LOCATION	BMP #	DRAINAGE AREA (ACRES)	ANNUAL TN LOAD (LBS)	ANNUAL TN LOAD REDUCTION (LBS)	% LOAD REDUCTION	\$/LBS NITROGEN
WINTER	1	12.88	90.1	68.2	76%	\$680
STREET	2*	24.56	157.6	120.2	76%	\$660
	3.1	0.20	2.5	2	80%	\$4,000
	3.2	0.13	1.7	1.3	76%	\$5 <i>,</i> 080
	3.3	0.27	3.4	2.6	77%	\$4,620
	3.4	0.22	2.9	2.9 2.2 77%		\$4,500
LINCOLN	3.5	0.24	2.4	1.8	75%	\$3 <i>,</i> 890
STREET NORTH	3.6	0.78	7.2	5.7	79%	\$3,830
	3.8	1.20	9.1	7.1	78%	\$3,100
	3.9	0.70	5.6	4.2	75%	\$3,240
	3.22	0.20	1.3	1.0	74%	\$3,000
LINCOLN	3.20	1.60	13.9	10.7	77%	\$3,090
STREET SOUTH	3.21	0.24	1.4	1.0	72%	\$2,800
FRONT STREET	5	20.29	138.3	71.7	52%	\$640
Totals	-	63.5	437.5	299.7	69%	\$1,040

Table 3: Pollutant Load Reduction and Performance for Priority BMPs 1, 2, 3, and 5 for ½" Water Quality Volume

9. BMP FLOOD REDUCTION BENEFITS



The existing CAPE SWMM model was updated to include the proposed BMPs 1, 2, 3, and 5 in order to analyze the flood reduction benefits associated with the BMPs both from a standpoint of flood duration (using the SWMM 1-D model) and flooding extent (using the PCSWMM 2-D model) during a 10-year, 24-hour storm event. Results from this analysis are presented in Figure 19, Figure 20, and Figure 21.

Although none of the BMPs are designed to manage a 10-year storm (4.72" of runoff; each BMP is designed to handle 0.5" of runoff with BMP 5 designed to manage 0.25"), modeling results indicate that they will have a significant impact on flood duration at 12 major catch basins and manholes, as well as flood extent reductions at many key locations within the Lincoln Street watershed.

Results inidcate a 5 million gallon decrease in total runoff (25% reduction) during the 10-year, 24-hour storm event following installation of the recommended suite of BMPs. This translates to significant flooding extent reduction benefits along railroad avenue (just downstream of BMPs 1 and 2), along Lincoln Street (just downstream of BMPs 3.1-3.22), and along Front Street (just upstream of BMP 5). The flood reduction benefits are expected to be even more significant during smaller, more frequent storm events that are common flooding in the Town of Exeter.



Figure 19: Modeled Flood Reduction Impacts of BMPs 1 and 2 (sized for 1/2" WQV)



Figure 20: Modeled Flood Reduction Impacts of BMP 3 (sized for 1/2" WQV)



Figure 21: Modeled Flood Reduction Impacts of BMP 5 (sized for 1/4" WQV)

10. ENGINEERING COST ESTIMATES



A costing analysis was performed to quantify the total and unit costs (cost per pound of nitrogen removed) for each BMP. Engineering cost estimates were developed based on materials quantities, labor, and equipment for BMPs 1, 2, 3, and 5 and are shown in Table 4. A more detailed look at the costing analysis is provided in Appendix G: Engineering Cost Estimates.

Of particular note is the low unit costs (\$ per pound of nitrogen loading reduction) associated with the subsurface infiltration systems (BMPs 1, 2, and 5). For all three of these systems, the unit cost is estimated at well below \$1,000, representing an extremely economical option for reducing nitrogen loading in the Lincoln Street watershed. BMPs 1, 2, and 5 all manage runoff from large drainage areas, making it possible to achieve economies of scale not possible for BMPs 3.1-3.22. These ROW infiltration and tree planter systems have relatively small drainage areas (< 2 acres) meaning they will each handle fairly small nitrogen loads. Nevertheless, \$3,000-\$5,000 (the unit cost per pound of nitrogen loading reduction associated with BMPs 3.1-3.22) is still a worthwhile expenditure, especially given that each of these systems is expected to control around ³/₄ of the total nitrogen load from their respective drainage areas.

Tremendous cost saving opportunities exist when BMP retrofits are timed with road and utility improvements. For example, a bioretention system designed to treat 1 acre of runoff might cost an estimated \$40,000. However, when paired with road improvements the costs may be reduced to \$10,000 due to the shared costs of curbs, sidewalks, and roads.

Table 4: Engineering Cost Estimates for BMPs 1, 2, 3, and 5

LOCATION	BMP #	DRAINAGE AREA (ACRES)	ANNUAL TN REDUCTION (LBS)	% LOAD REDUCTION	95% DESIGN COST ESTIMATE	\$/LBS NITROGEN
WINTER STREET	1	12.9	68.2	76%	\$45,900	\$680
	2	24.6	120.2	76%	\$79,000	\$660
Subtotal	-	37.4	188.4	76%	\$124,900	-
	3.1	0.2	2.0	80%	\$8,000	\$4,000
	3.2	0.1	1.3	76%	\$6,600	\$5,080
	3.3	0.3	2.6	77%	\$12,000	\$4,620
LINCOLN STREET	3.4	0.2	2.2	77%	\$9,900	\$4,500
NORTH	3.5	0.2	1.8	75%	\$7,000	\$3,890
	3.6	0.8	5.7	79%	\$21,800	\$3,830
	3.8	1.2	7.1	78%	\$22,000	\$3,100
	3.9	0.7	4.2	75%	\$13,600	\$3,240
	3.22	0.2	1.0	77%	\$3,000	\$3,000
Subtotal	-	3.9	27.9	77%	\$103,900	-
LINCOLN STREET	3.20	1.6	10.7	77%	\$33,000	\$3,090
SOUTH	3.21	0.2	1.0	72%	\$2,800	\$2,800
Subtotal	-	1.8	11.7	76%	\$35,800	-
FRONT STREET	5	20.3	71.7	52%	\$45,200	\$640
Total	_	63.5	299.7	69%	\$309,800	-

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A detailed Operations and Maintenance Plan has been developed for the proposed BMPs and is provided in Appendix H: Operations and Maintenance Plan. This includes methods, checklists, and annual reporting forms. All BMPs will incorporate low maintenance design elements with an emphasis on pre-treatment to reduce maintenance needs. A series of maintenance fact sheets and recommendations are also provided in Appendix H for tree planters, right-of-way infiltration, and subsurface infiltration. The focus on pretreatment will provide easy-to-maintain shallow sumps for collection of sediment and trash with standard maintenance procedures using vactor trucks and requires no specialty equipment or training. The location of curb cuts will be spaced to optimize the function of existing drainage infrastructure.

To ensure the effectiveness of BMPs, regular inspections and maintenance is necessary. Generally speaking, inspection and maintenance falls into two categories: expected routine maintenance and non-routine (repair) maintenance. Routine maintenance is performed regularly to maintain both aesthetics and good working order of BMPs. Routine inspection and maintenance helps prevent potential nuisances (odors, mosquitoes, weeds, etc.), reduces the need for repair maintenance, and insures long term performance.

Under MS4 rules, owners and operators are responsible for implementing BMP inspection and maintenance programs and having penalties in place to deter infractions. The rules recommend that all stormwater BMPs should be inspected on a regular basis for continued effectiveness and structural integrity.

12. OUTREACH EFFORTS



Public outreach and education is a critical component of raising awareness and building support for resiliency and water infrastructure management within any community. The project team attended two meetings and presented interim and final project findings to the Conservation Commission. The commission was very supportive of the efforts and an engaging discussion was had regarding the potential benefits and long-term implications. The presentations are available in Appendix F: Outreach Efforts

13. RECOMMENDATIONS



As part of a future Phase II effort, we recommend pursuing further analyses to identify additional potential BMPs to maximize flood reduction along Tan Lane and further reduce nutrient loading. This examination should include the following areas: 1) BMP 4 in the vicinity of Lincoln Street School and Kiminees Brook which has been covered and piped in the ravine area, 2) BMP 7 areas draining the south end of Lincoln Street feeding a major storm drain that joins item #1 and #3, 3) BMP 8 for areas draining Front Street and Elm Street, and 4) BMP 9 for areas draining Main Street and Tan Lane. BMPs installed in these locations would likely have substantial flood reduction and water quality benefits given that they represent most of the major trunklines (including Phase I) within the S10 watershed.

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15. APPENDICES



APPENDIX A: DRAINAGE INFRASTRUCTURE INVENTORY AND LAND USE APPENDIX B: SOIL TEST PIT RECORDS APPENDIX C: ASSUMPTIONS AND LIMITATIONS APPENDIX D: WATERSHED MODELING METHODOLOGY APPENDIX E: POLLUTANT LOAD METHODOLOGY APPENDIX F: OUTREACH EFFORTS APPENDIX G: ENGINEERING COST ESTIMATES APPENDIX H: OPERATIONS AND MAINTENANCE PLAN APPENDIX I: 95% BMP DESIGN PACKAGE APPENDIX A: DRAINAGE INFRASTRUCTURE INVENTORY AND LAND USE



Project Name: Lincoln Street Phase I Project Number: 16928 Client: Town of Exeter Date: 25-Nov-16

Exeter Drainage **Rim Elevation** Invert Elevation Diameter **Total Depth** DPW ID Invert Depth (in) Date / Time Pipe ID Pipe Type Entry # Inspector Notes Inventory ID (ft) (ft) (in) (in) Primary Influent 88 52.2 RCP 18 Secondary Influent 60 54.5 RCP 12 DMH-0899 11/17/16 11:00 AM 1 A. Moskal MH34 59.5 75 Primary Effluent 95 51.6 RCP 18 Primary Influent 75 53.1 RCP 14 78 52.8 RCP 14 Primary Effluent DMH-0902 11/17/16 11:00 AM A. Moskal 2 MH36 59.3 60 Secondary Influent 64 54.0 RCP 12 Secondary Influent 73 53.2 RCP 12 Primary Influent 81 53.05 RCP 14 Primary Effluent 52.9 RCP 14 83 3 DMH-0904 11/17/16 11:00 AM MH40 59.8 A. Moskal 66 Primary Influent 81 53.85 RCP 14 Primary Effluent 53.7 RCP 83 14 4 DMH-0905 11/17/16 11:00 AM A. Moskal MH39 60.6 66 Primary Influent 115 49.4 RCP 18 Primary Effluent RCP 121 48.9 24 5 DMH-0897 11/17/16 11:00 AM A. Moskal MH41 59 96 Secondary Influent 107 50.1 RCP 14 Primary Influent 132 48.4 RCP 24 Primary Effluent 134 48.2 RCP 24 DMH-0895 11/17/16 11:00 AM A. Moskal MH43 59.4 117 6 Secondary Influent 58 54.6 PVC 12 Primary Influent 120 33.3 RCP 14 Primary Effluent 121 33.2 RCP 14 7 DMH-0777 11/17/16 11:00 AM A. Moskal MH48 43.3 115 Secondary Influent 61 38.2 RCP 12 Primary Influent 121 33.3 RCP 14 Primary Effluent 122 33.2 RCP 14 DMH-0778 11/17/16 11:00 AM MH47 8 A. Moskal 43.4 116 RCP Primary Influent 129 32.7 14 Primary Effluent 131 32.5 RCP 14 9 DMH-0801 11/17/16 11:00 AM A. Moskal MH50 43.4 124 Secondary Influent 81 36.7 RCP 12 135 30.85 RCP Primary Influent 14 Primary Effluent 136 30.8 RCP 14 10 DMH-0804 11/17/16 11:00 AM A. Moskal MH52 42.1 115 Secondary Influent 84 35.1 RCP 12 INSPECTION KEY: RCP: Reinforced Concrete, PVC: Polyvinyl Chloride

Manhole Inspection Results

OBSERVATIONS: Total Depth of all structures can be assumed as the invert of the primary effluent; total depth recorded is to the flat base above the bottom pipe

Adam Moskal Performed By

Reviewed By

<u>11/17/2016</u> Date

11/25/2016 Date



Project Name: Lincoln Street Phase I Project Number: 16928 Client: Town of Exeter

Date: 25-Nov-16

Catch Basin Inspection Results

Entry #	Exeter Drainage Inventory ID	Date / Time	Inspector	Exeter DPW ID	Pipe ID	Rim Elevation (ft)	Invert Depth (in)	Invert Elevation (ft)	Pipe Type	Diameter (in)	Total Depth (in)	Notes
					Primary Influent		121	49.8	RCP	12		
					Primary Effluent		124	49.6	RCP	18		
1	CB-0959	11/17/16 11:00 AM	A. Moskal	CB31		59.9					124	
					Primary Influent		102	50.9	RCP	18		
2	CD 0059	11/17/16 11:00 AM	A Mashal	CD22	Primary Effluent	50.4	104	50.7	RCP	18	104	
2	CB=0958	11/17/10 11:00 AM	A. WOSKAI	6832		39.4	-				104	
					Primary Influent							
					Primary Effluant		42	55.2	PCP	12		
3	CB-0900	11/17/16 11:00 AM	A. Moskal	CB33	Fillinary Elindent	58.8	45	33.2	KCI	12	82	
					Primary Influent		96	50.9	RCP	14		
	CD 0000			GD 30	Primary Effluent	50.0	98	50.7	RCP	14		
4	CB-0898	11/1//16 11:00 AM	A. Moskal	CB38		58.9					98	
					Primary Influent		117	49.0	RCP	24		
					Primary Effluent		118	48.9	RCP	24		
5	CB-0896	11/17/16 11:00 AM	A. Moskal	CB42	T Timle y Estimetin	58.7	110	105	iter	21	118	
					Primary Influent		40	57.2	RCP	12		
6	CB 0804	11/17/16 11:00 AM	A Mashal	CD 14	Primary Effluent	60 565	44	56.9	RCP	12	44	
0	CD-0894	11/1//10 11:00 AIM	A. WOSKAI	CB44		60.565					44	
					Primary Influent		100	53.4	RCP	14		
-	GD 0057			GD 30	Primary Effluent		103	53.1	RCP	14	102	
7	CB-0956	11/1//16 11:00 AM	A. Moskal	CB30	Secondary Influent	61.7	60	56.7	RCP	12	103	
8	CB-0776	11/17/16 11:00 AM	A. Moskal	CB49	Primary Effluent	43	38	39.8	RCP	12	78	
9	CB-0802	11/17/16 11:00 AM	A Moskal	CB46	Primary Effluent	44.4	76	38.1	RCP	12	113	
ŕ												
					Primary Influent		69	37.4	RCP	12		
10	CB-0803	11/17/16 11:00 AM	A. Moskal	CB53	Primary Effluent	43.1	70	37.3	RCP	12	70	
11	CB-0805	11/17/16 11:00 AM	A. Moskal	CB51	Primary Effluent	42.3	44	38.6	RCP	12	86.5	

INSPECTION KEY: RCP: Reinforced Concrete, PVC: Polyvinyl Chloride

OBSERVATIONS: Total Depth of all structures can be assumed as the invert of the primary effluent; total depth recorded is to the base of the flat base above the bottom pipe

Rind Da Reviewed By

Adam Moskal Performed By 11/17/2016 Date

11/25/2016 Date

BMP 2

Drainage infrastructure near BMP 2 was evaluated for retrofit feasibility and checked for invert elevations of pipes, direction of flow, and pipe characteristics. Figure 22 displays the location of the drainage infrastructure adjacent to BMP 2 that was assessed during a site visit. Figure 23 shows the drainage infrastructure elevations with the colored rectangles representing each individual structure. This examines the feasibility of rerouting certain storm drains to treatment systems without flooding upstream catch basins or manholes. For BMP 2, this would involve the installation of a weir at the junction of Columbus Ave. and Winter St. (MH41) that would reroute drainage from Columbus Ave to a subsurface infiltration system located at the corner of Railroad Ave and Winter Street in the outlined area. Complete drainage structure inventory records can be found in Appendix A of this document.



Figure 1: BMP 2 Subsurface Infiltration at Winter Street, Columbus Avenue, and Railroad Avenue



Figure 2: BMP 2 Drainage Elevations

BMP 5

Drainage infrastructure near BMP 5 was evaluated for retrofit feasibility and surveyed for pipe invert elevations, direction of flow, and pipe characteristics. Figure 24 displays the location of the drainage infrastructure adjacent to BMP site 5 that were assessed during a site visit. Figure 25 shows the drainage infrastructure elevations with the colored rectangles representing each individual structure. This examines the feasibility of rerouting certain storm drains to treatment systems without flooding upstream catch basins or manholes. At site 5, a weir would be installed at the junction of Front St. and Tan Ln. (see MH52) that would reroute drainage into a ROW Infiltration/Filtration system located in the outlined area. Complete drainage structure inventory records can be found in Appendix A of this document.



Figure 3: BMP Site 5 at Front Street, Tan Lane, and Elliot Street



Figure 4: BMP Site 5 Drainage Elevation

	Hydrologic Soil	Area	Annual Nitrogen Export
Land Use Type	Group*	(acres)	(lbs)**
Agriculture	А	0.04	0.02
Agriculture	C/D	0.47	1.51
Commercial, Services, and			
Institutional	А	6.44	3.42
Commercial, Services, and			
Institutional	C/D	15.48	41.48
Commercial, Services, and			
Institutional	IMP	30.72	424.48
Forest	А	3.62	1.01
Forest	C/D	2.69	3.88
Forest	IMP	0.02	0.27
Industrial and Commercial Complexes	C/D	0.00	0.01
Industrial and Commercial Complexes	IMP	0.77	10.64
Outdoor and Other Urban and Built-			
up Land	А	1.83	2.00
Outdoor and Other Urban and Built-			
up Land	C/D	6.15	34.07
Outdoor and Other Urban and Built-			
up Land	IMP	0.48	6.62
Residential	А	20.41	10.82
Residential	C/D	47.59	127.53
Residential	IMP	26.26	413.04
Transitional	А	0.09	0.02
Transitional	C/D	0.23	0.31
Transitional	IMP	0.19	2.68
Transportation, Communications, and			
Utilities	А	0.16	0.04
Transportation, Communications, and			
Utilities	C/D	0.14	0.17
Transportation, Communications, and			
Utilities	IMP	16.17	182.87
Total		179	1265

Table 1: Lincoln Street Total Land Use Watershed Characteristics

* Hydrologic soil group derived from landform. Watershed area was divided into 3 slope classes, 0-3%, 3-8%, and 8-15%. Dominant soil type for each slope class was assumed for entire slope class. Scitico silt loam for 0-3% slopes, Charlton fine sandy loam for others. **Based on WISE, 2015 PLERs

Land Use Type	Hydrologic Soil	Area	Annual Nitrogen Export		
	Group*	(acres)	(lbs)**		
Agriculture	А	0.04	0.02		
Agriculture	C/D	0.47	1.51		
Commercial, Services, and Institutional	A	0.18	0.09		
Commercial, Services, and Institutional	C/D	1.91	5.13		
Commercial, Services, and Institutional	IMP	5.21	70.87		
Outdoor and Other Urban and Built- up Land	A	0.04	0.04		
Outdoor and Other Urban and Built- up Land	C/D	2.81	15.59		
Outdoor and Other Urban and Built- up Land	IMP	0.39	5.37		
Residential	A	5.87	3.11		
Residential	C/D	24.97	66.91		
Residential	IMP	10.43	164.11		
Transportation, Communications, and Utilities	A	0.00	0.00		
Transportation, Communications, and Utilities	C/D	0.05	0.06		
Transportation, Communications, and Utilities	IMP	5.12	57.91		
Total		57	390		

Table 2: Lincoln Street Land Use Upper Watershed Characteristics

* Hydrologic soil group derived from landform. Watershed area was divided into 3 slope classes, 0-3%, 3-8%, and 8-15%. Dominant soil type for each slope class was assumed for entire slope class. Scitico silt loam for 0-3% slopes, Charlton fine sandy loam for others. **Based on WISE, 2015 PLERs

Land Use Type	Hydrologic Soil	Area	Annual Nitrogen Export
	Group*	(acres)	(lbs)**
Commercial, Services, and Institutional	A	6.27	3.32
Commercial, Services, and Institutional	C/D	13.56	36.35
Commercial, Services, and Institutional	IMP	25.51	353.61
Forest	А	3.62	1.01
Forest	C/D	2.69	3.88
Forest	IMP	0.02	0.27
Industrial and Commercial Complexes	C/D	0.00	0.01
Industrial and Commercial Complexes	IMP	0.77	10.64
Outdoor and Other Urban and Built-up	A		
Land		1.80	1.96
Outdoor and Other Urban and Built-up	C/D	2 2 2	10.40
		5.55	18.48
Outdoor and Other Urban and Built-up Land	IMP	0.09	1.25
		4454	
Residential	А	14.54	7./1
Residential	C/D	22.62	60.62
Residential	IMP	15.82	248.93
Transitional	А	0.09	0.02
Transitional	C/D	0.23	0.31
Transitional	IMP	0.19	2.68
Transportation, Communications, and	A		
Utilities		0.16	0.04
Transportation, Communications, and Utilities	C/D	0.09	0.11
Transportation, Communications, and	IMP		
Utilities		11.05	124.96
Total		122	876

Table 3: Lincoln Street Land Use Lower Watershed Characteristics

* Hydrologic soil group derived from landform. Watershed area was divided into 3 slope classes, 0-3%, 3-8%, and 8-15%. Dominant soil type for each slope class was assumed for entire slope class. Scitico silt loam for 0-3% slopes, Charlton fine sandy loam for others. **Based on WISE, 2015 PLERs

SCOUR VELOCITY ANALYSIS

The following tables display the pipe velocities in the vicinity of BMPs 1, 2, and 5 under baseline conditions (no weirs or BMPs added) and proposed conditions. Each row of the table represents a reach of pipe between a listed in and out junction. Weir locations are noted in the left-hand columns of each table.

Junction	Junction	Pipe	Pipe	Flow Rate	Velocity					
In	Out	Length	Diameter	(cfs)	(fps)	Scenario				
	Main Sewer Line Entry to BMP 1, BMP 2									
140	120	202	15"	2.06	3.12	w/ weir				
J40	123	502	12	2.01	3.32	w/o weir				
120		106	10"	3.19	2.71	w/ weir				
123	CB-0952	100	18	3.3	2.98	w/o weir				
		214	10	3.95	3.06	w/ weir				
CB-0952	DIVIH-0954	214	18	4.8	3.37	w/o weir				
	CB-0955	100	10	4.62	2.62	w/ weir				
DIVIH-0954	(BMP 1 Weir)	180	18	5.47	4.26	w/o weir				
CB-0955		225	10"	1.22	4.15	w/ weir				
(BMP 1 Weir)	CB-0920	325	10	5.33	6.24	w/o weir				
		215	1.011	1.67	4.32	w/ weir				
CB-0926	CB-0928	215	18	5.78	6.01	w/o weir				
		45	10"	2.42	2.79	w/ weir				
CB-0958	CB-0929	45	18	6.23	4.92	w/o weir				
	DMH-0897	04	10	2.75	1.56	w/ weir				
CB-0959	(BMP 2 Weir)	94	18	6.38	3.61	w/o weir				
DMH-0897	122	110	2.41	2.13	2.11	w/ weir				
(BMP 2 Weir)	133	110	24	12.63	4.02	w/o weir				
		North	Sewer Line Entr	y to BMP 2						
124	122	222	15"	3.73	4.7	w/ weir				
131	J32	322	15"	3.73	4.7	w/o weir				
122	DMH-0897	120	15"	7.01	6.33	w/ weir				
J32	(BMP 2 Weir)	128	15	7.16	6.35	w/o weir				

 Table 4 - Pipe velocities in vicinity of BMPs 1 and 2

Junction In	Junction Out	Pipe Length	Pipe Diameter	Flow Rate (cfs)	Velocity (fps)	Scenario	
West Sewer Line Entry to J129							
1120	1120	705	10"	1.24	3.85	w/ weir	
1130	J129	705	12	1.56	3.29	w/o weir	
1120	J127	150	10"	6.64	3.76	w/ weir	
J129	(BMP 5 Weir)	120	18	5.74	4.77	w/o weir	
J127	1124	E10	10"	5.77	5.79	w/ weir	
(BMP 5 Weir)	J124	518	18	8.38	9.13	w/o weir	
		South	Sewer Line Ent	ry to J129			
1122	11.2.1	421	15"	2.1	2.86	w/ weir	
J132	1121	421	12	2.09	2.86	w/o weir	
1121	11.2.9	104	15"	2.65	3.61	w/ weir	
1121	J128	184	12	2.66	3.82	w/o weir	
1120	1120	75	15"	5.64	4.59	w/ weir	
J128	1129	/5	12	4.94	4.7	w/o weir	

 Table 5 - Pipe velocities in vicinity of BMP 5
 Image: Comparison of the second sec

APPENDIX B: SOIL TEST PIT RECORDS

Table 1: Soil Coring Findings

BMP #	Location	Soil Type	Hydrologic Soil Group	Saturated Hydraulic Conductivity (in/hr)	ВМР Туре
1	Playground on the intersection of Winter St. and Front St.	62B: Charlton Fine Sandy Loam	A	0.6-6	Subsurface Infiltration
2	Intersection of Columbus Ave., Winter St., and Railroad Ave.	62B: Charlton Fine Sandy Loam	A	0.6-6	Subsurface Infiltration
3	24 Lincoln Street	62B: Charlton Fine Sandy Loam	A	0.6-6	ROW Infiltration/Filtration
4	Lincoln Street Elementary School Parking Lot	62B: Charlton Fine Sandy Loam	A	0.6-6	Subsurface Infiltration
5	Philips Exeter Academy	62B: Charlton Fine Sandy Loam	A	0.6-6	Subsurface Infiltration
6	Intersection of Washington St. and Spruce St.	33A Scitico Silt Loam	C/D	0-0.2	ROW Infiltration/Filtration
7	Lincoln Street Elementary School Playground	62B: Charlton Fine Sandy Loam	A	0.6-6	Subsurface Infiltration

Soil Test Pit Worksheet



Project Name: Linco	oln	Street Phase I	Date: 11/28/2016					
Project Number: 16	592	8	Technic	ian: A. Mos	skal, M. Rose	en		
Location: TP1 Inters	sec	tion of Railroad Ave., Winter St., and Columbus Ave.	Descrip	tion: Soil Pi	it by Auger			
						ТР		
Horizons		Layer	Depth (in)	Color	Texture	SHWT	Roots	Notos
			inches	COIOI	Consistency	yes, no, depth	inches	Notes
more all and a second s		O – Top layer, "organic" layer	0-4	Black	Organics	No		62B: Charlton Fine Sandy Loam, 3-8% Slopes
	1	A – Second layer of soil, "top soil", lots of organic matter mixed, darkly colored.	4-22	2.5y 4/1	Fine Loamy Sand	No		
	-	B – Subsoil layer. Transition between top soil and subsoil. Striations and repeating floodplain deposition layers	B1: 22-28 B2: 28-42	B1: 2.5y 5/4 B2: 2.5y 6/4	Fine Loamy Sand	No		
		C – This layer usually has lots of large rocks mixed in with deep soil.	C1: 42-54 C2: 54+	C1: 5y 7/2 C2: 5y 8/1	C1: Sandy Loam C2: Sand	No		
	D – Bedrock							
Project Name: Linco	oln	Street Phase I	Date: 12/06/2016					
Project Number: 16	592	8	Technic	Fechnician: A. Moskal, M. Roseen				
Location: TP2 (Play	gro	und adjacent to Winter St. and Front St. Intersection)	Descrip	tion: Soil Pi	it by Auger			
				1	1	TP	1	
Horizons		Layer	Depth (in)	Calar	Texture	SHWT	Roots	Notes
			inches	COIOI	Consistency	yes, no, depth	inches	Notes
=	ł_	0 – Top layer, "organic" layer	0-3	Black	Heavy Organic	No		62B: Charlton Fine Sandy Loam, 3-8% Slopes
=	ŀ	A – Second layer of soil, "top soil", lots of organic matter mixed, darkly colored.	3-8	10 yr 4/4	Fine Loamy Gravely Sand	No		
	-	B – Subsoil layer. Transition between top soil and subsoil. Striations and repeating floodplain deposition layers	B1: 8-22 B2: 22-35	B1: 10y 6/6 B2: 2.5y 7/4	Fine Loamy Sand	No		
		C – This layer usually has lots of large rocks mixed in with deep soil.	41+	2.5y 7/3	Fine Silty Loam	No		
		D – Bedrock						

Project Name: Lin	coln	Street Phase I	Date: 11/28/2016								
Project Number: :	1692	8	Technician: A. Moskal, M. Roseen								
Location: TP3 (Int	erse	ction of Washington and Spruce)	Description: Soil Pit by Auger								
			ТР								
Horizons		Layer	Depth (in)		Texture	SHWT	Roots				
			inches	Color	Consistency	yes, no, depth	inches	Notes			
man have a]-	O – Top layer, "organic" layer	0-6	Black	Organics	No		33A Scitico Silt Loam 0 to 5 % Slopes			
]	A – Second layer of soil, "top soil", lots of organic matter mixed, darkly colored.	6-12	5y 4/2	Fine Loamy Sand	No					
° ° ° °	-	B – Subsoil layer. Transition between top soil and subsoil. Striations and repeating floodplain deposition layers	B1: 12-19 B2: 19+	В1: 5у 5/2 В2: 5у 5/1	B1: Sandy Loam B2: Silty Clay	No		No significant change after 19"			
		 C – This layer usually has lots of large rocks mixed in with deep soil. 		5y 5/1	Silty Clay	No					
		D – Bedrock									
Project Name: Lin	coln	Street Phase I	Date: 12/06/2016								
Project Number: :	1692	8	Technician: A. Moskal, M. Roseen								
Location: TP4 (24	Linc	oln Street)	Description: Soil Pit by Auger								
				1	-	TP	1				
Horizons		Layer	Depth (in)	Calar	Texture	SHWT	Roots	Neter			
			inches	COIOI	Consistency	yes, no, depth	inches	Notes			
my Marine	}	O – Top layer, "organic" layer	0-2	Black	Heavy Organic	No		62B: Charlton Fine Sandy Loam, 3-8% Slopes			
	ŀ	A – Second layer of soil, "top soil", lots of organic matter mixed, darkly colored.	2-14	5y 4/1	Fine Loamy Sand	No					
		B – Subsoil layer. Transition between top soil and subsoil. Striations and repeating floodplain deposition layers	B1: 14-18 B2: 18-32	B1: 5y 4/2 B2: 2.5y 8/1	B1: Sandy Loam B2: Fine Loamy Sand	No					
		C – This layer usually has lots of large rocks mixed in with deep soil.	32+	7.5yr 5/4	Fine Loamy Sand	No					
	7	D – Bedrock									

Soil Test Pit Worksheet



Project Name: Lincoln Street Phase I		Date: 12/06/2016					
Project Number: 16928 Location: TP5 Valley Bottom behind Lincoln Street Elementary School Parking Lot		Technician: A. Moskal, M. Roseen Description: Soil Pit by Auger					
Horizons	Layer	Depth (in) inches	Color	Texture Consistency	SHWT	Roots	Notes
					yes, no, depth	inches	
	0 – Top layer, "organic" layer	0-5	Black	Heavy Organic	No		62B: Charlton Fine Sandy Loam, 3-8% Slopes
	A – Second layer of soil, "top soil", lots of organic matter mixed, darkly colored.	5-14	7.5 yr 4/1	Loamy Sand with Gravel	No		
	B – Subsoil layer. Transition between top soil and subsoil. Striations and repeating floodplain deposition layers	B1: 14-20 B2: 20+	B1: 5y 4/2	Saturated Loamy Sand	Yes: 26 in		Could not sample any deeper
	C – This layer usually has lots of large rocks mixed in with deep soil.						
	D – Bedrock						
Project Name: Lincoin Street Phase I		Date: 12/0//2016					
Project Number: 16928		Tochnic	2/07/2016	kal M Roso			
Location: TP6 (In front	8 of Philins Eveter Academy)	Technic	2/07/2016 ian: A. Mos	ikal, M. Rose	en		
Location: TP6 (In front	8 : of Philips Exeter Academy)	Technic Descrip	2/07/2016 ian: A. Mos tion: Soil Pi	ikal, M. Rosed	en		
Location: TP6 (In front	8 : of Philips Exeter Academy)	Technic Descrip	2/07/2016 ian: A. Mos tion: Soil Pi	skal, M. Rosed it by Auger Texture	en TP SHWT	Roots	
Location: TP6 (In front Horizons	8 c of Philips Exeter Academy) Layer	Descrip Descrip Depth (in) inches	2/07/2016 ian: A. Mos tion: Soil Pi	ikal, M. Rosee it by Auger Texture Consistency	en TP SHWT yes, no, depth	Roots	Notes
Location: TP6 (In front Horizons	8 c of Philips Exeter Academy) Layer O – Top layer, "organic" layer	Descrip Descrip Depth (in) inches	2/07/2016 iian: A. Mos tion: Soil Pi Color Black	it by Auger Texture Consistency Heavy Organic	en TP SHWT yes, no, depth No	Roots	Notes 62B: Charlton Fine Sandy Loam, 3-8% Slopes
Location: TP6 (In front Horizons	8 c of Philips Exeter Academy) Layer 0 – Top layer, "organic" layer A – Second layer of soil, "top soil", lots of organic matter mixed, darkly colored.	Technic Descrip Depth (in) inches 0-2 2-9	2/07/2016 iian: A. Mos tion: Soil Pi Color Black 10yr 5/3	it by Auger Texture Consistency Heavy Organic Loamy Sand with Gravel	en TP SHWT yes, no, depth No No	Roots	Notes 62B: Charlton Fine Sandy Loam, 3-8% Slopes
Location: TP6 (In front Horizons	8 c of Philips Exeter Academy) Layer 0 – Top layer, "organic" layer A – Second layer of soil, "top soil", lots of organic matter mixed, darkly colored. B – Subsoil layer. Transition between top soil and subsoil. Striations and repeating floodplain deposition layers	Date: 1 Technic Descrip Depth (in) inches 0-2 2-9 81: 9-16 B2: 16-28 16-28	2/07/2016 iian: A. Mos tion: Soil Pi Color Black 10yr 5/3 B1: 10yr 6/8 B2: 2.5y 8/4	it by Auger Texture Consistency Heavy Organic Loamy Sand with Gravel Fine Loamy Sand	en TP SHWT yes, no, depth No No	Roots inches	Notes 62B: Charlton Fine Sandy Loam, 3-8% Slopes
Location: TP6 (In front	8 C – This layer usually has lots of large rocks mixed in with deep soil. C – This layer usually has lots of large rocks mixed in with deep soil.	Date: 1 Technic Descrip Depth (in) inches 0-2 2-9 B1: 9-16 B2: 16-28 28+	2/07/2016 ian: A. Mos tion: Soil Pi Color Black 10yr 5/3 B1: 10yr 6/8 B2: 2.5y 8/4 10yr 8/4	Skal, M. Rosee it by Auger Texture Consistency Heavy Organic Loamy Sand With Gravel Fine Loamy Sand Fine Loamy Sand	en TP SHWT yes, no, depth No No No	Roots inches	Notes 62B: Chariton Fine Sandy Loam, 3-8% Slopes
APPENDIX C: ASSUMPTIONS AND LIMITATIONS

ASSUMPTIONS AND LIMITATIONS

All watershed models seek to represent complex physical processes through the use of simplifying equations and assumptions. The process of parameterizing watershed characteristics to suit a watershed model involves an inherent level of uncertainty. Though it is impossible to avoid this uncertainty, it is important to understand the sources of uncertainties so that they can be quantified and incorporated into the model to create a more robust analysis. The sources of uncertainty in this analysis are described below along with a brief discussion of the main approaches for characterizing the uncertainty of the model input parameters. The sources of uncertainty relating to the model input parameters arise from, but are not limited to, the:

- Representativeness of data from studies conducted in other areas that were used in the analysis (e.g. runoff concentrations).
- General uncertainty in any stormwater data due to measurements, field protocols, data quality, and data accuracy.
- Stormwater volume estimation methods that rely on empirical relationships between annual rainfall and runoff.
- Spatial uncertainty in watershed/site conditions (e.g., imperviousness, soils, runoff parameters), as they relate to the certainty that can be had regarding hydrologic conditions at a given location.
- Model output relates one land use to one nutrient management measure and therefore, cannot be applied to a variety of land uses or multiple consecutive nutrient management measures (i.e., treatment train).
- Model output associated with runoff volume and pollutant load are scaled from 1-acre parcels to the entire watershed area.
- Model does not consider runoff hydraulics after runoff leaves a hydrologic response unit or nutrient management measure.

It is important to note that the model does not seek to describe the temporal variability that is inherent in stormwater pollutant loading. The model is intended to estimate long-term average conditions for the location and project. At this scale, temporal variability (e.g., storm-to-storm, year-to-year) is not relevant. Additionally, the model is not intended to predict conditions for a given storm event or monitoring period.

The previously mentioned assumptions are more or less general to all watershed modeling studies. Some further assumptions of note that are specific to this effort are:

- Design storm rainfall volumes based on data from the NRCC for Exeter, NH.
- Subcatchment runoff characteristics for current conditions are based on 2005 land use data, the most current available data set.
- Infiltration/runoff calculations are based on the least sophisticated method available in PCSWMM (CN vs. CN + Imp. Green-Ampt, or Horton methods).

- The representations of BMPs 1, 2, 3, and 5 in the PCSWMM model mimic the intended *function* of the systems they represent (e.g. storage capacity for 0.5" of runoff depth before bypassing) but many of the more specific *form* details associated with each system were unable to be represented due to limitations in the modeling software. Designs for the BMPs were based primarily on a HydroCAD modeling effort, though the PCSWMM model was used to quantify runoff reduction impacts at the watershed scale.
- Due to the number of catch basins, manholes, pipes and outfalls, Geosyntec developed a methodology under the CAPE project to accurately model the storm sewer infrastructure by reducing the number of nodes within the model to only represent the main trunk lines of the system. Based on this approach, catch basins and manholes in the model were represented at inlets, outlets, and areas where there was a change in pipe diameter. Drainage areas were delineated for the areas which drained to these pipes. This approach provides an accurate representation of the capacity of the system; however, does not include analysis of single catch basins and associated pipes which convey flows to the main trunk line. The modeling approach and analysis provides a conservative estimate of the system and represents the flow in the pipe at its maximum value along the length of the run, rather than gradually increasing flow as each catch basin downstream successively contributes to the system.
- The original CAPE model was not re-calibrated after adding BMPs 1, 2, 3, and 5 as no other major modifications to the original model were made.

APPENDIX D: WATERSHED MODELING METHODOLOGY

FLOOD MODELING

The flood modeling effort for the Lincoln Street Watershed Analysis built on an existing drainage model ("Model") developed as part of the Climate Adaptation Plan for Exeter (CAPE). The CAPE Model was modified to simulate the addition of BMPs 1, 2, 3, and 5 in order to determine the flood reduction impacts associated with these BMPs during the 10-year, 24-hour storm event (for which the CAPE Model was calibrated). The original CAPE Model development methodology is presented below, along with a section describing the modifications made for this assessment. It is important to note that the model was not recalibrated following the updates to the drainage network made as a part of the Lincoln Street Watershed Analysis.

Original CAPE Model Methodology¹

The Model was created using the US Environmental Protection Agency (USEPA) Storm Water Management Model (SWMM) modeling platform to evaluate the flooding potential of the stormwater infrastructure network under varying storm depths, tidal storm surge and future buildout conditions. The Model was used to investigate the flooding and surcharging of town storm drainage infrastructure during the 10-yr design storm event under a variety of conditions (such as climate change, land use/buildout changes, coastal storm surges, etc.). The Model was created for planning purposes and includes some simplifying assumptions; it is not intended to provide design parameters for stormwater infrastructure installation and/or replacement. Any preliminary stormwater infrastructure designs prepared by the Town of Exeter or its consultants should include independent detailed hydraulic/hydrologic analysis.

The Model framework consists of several components including: watershed drainage areas (i.e., storm sewered areas and non-sewered areas), storm sewer infrastructure network (i.e., catch basins, manholes, pipes and outfalls), and river segments (i.e., Little River and Exeter/Squamscott River).

Drainage Areas and Infrastructure Network

Two types of drainage areas were delineated for the Model, which included: areas where storm sewer infrastructure is present and areas where storm sewer infrastructure is not present. In the storm sewered areas, the drainage area or "sewershed" represents the areas draining to catch basins, manholes, culverts, pipes and outfalls (Figure 1). Areas where storm sewer infrastructure is not present, represent areas where stormwater follows natural drainage patterns and/or is intercepted by roadside swales and conveyed to receiving waters. These drainage areas were delineated using standard HUC-12 watersheds. In areas where a HUC-12 watershed intersected a delineated sewershed, the HUC-12 watershed was clipped so as to not overlap.

To delineate the drainage areas within the storm sewered area, Geosyntec obtained copies of Exeter Department of Public Works (DPW) storm sewer infrastructure logbooks as well as the current DPW GIS files of stormwater infrastructure. The GIS shapefiles contain location information for catch basins, manholes, culverts, and stormwater pipes, as well as pipe diameters. Rim elevations for catch basins and manholes were interpolated from LiDAR topographic data, with the inverts of any connecting pipes being located at an assumed depth from the rim. To supplement/confirm these assumptions, the DPW logbooks were used to modify pipe invert elevation where data was available. The data were assembled in ArcGIS

¹ Methodology and results are summarized in the memorandum prepared by Geosyntec Consultants, dated 21 October 2016, entitled "Storm Sewer Infrastructure Model Evaluation; 10-yr Design Storm Analysis; Exeter, New Hampshire"

and critical information (such as depth, invert, material, etc.) was transcribed from the logbooks into the shapefile attribute information.

Due to the number of catch basins, manholes, pipes and outfalls, Geosyntec developed a methodology under the CAPE project to accurately model the storm sewer infrastructure by reducing the number of nodes within the model to only represent the main trunk lines of the system. Based on this approach, catch basins and manholes in the model were represented at inlets, outlets, and areas where there was a change in pipe diameter. Drainage areas were delineated for the areas which drained to these pipes. This approach provides an accurate representation of the capacity of the system; however, does not include analysis of single catch basins and associated pipes which convey flows to the main trunk line. The modeling approach and analysis provides a conservative estimate of the system and represents the flow in the pipe at its maximum value along the length of the run, rather than gradually increasing flow as each catch basin downstream successively contributes to the system.

Geosyntec obtained American Recovery and Reinvestment Act (ARRA) LiDAR Data for the Northeast from the University of New Hampshire GRANIT spatial data distribution site. The primary use of the LiDAR topographic data was to delineate drainage areas and to determine approximate rim elevations of catch basins and manholes, as these were not readily available in the DPW data. Attachment 1 provides a map book of the delineated storm sewersheds.

River Segments

Cross sections of the river networks were modeled to understand the effects of backwater within the storm sewer network caused by water surface elevations in the receiving waters (i.e., Little River and Exeter Squamscott Rivers) related to the tidal cycle and coastal storm surge. To include this effect in the simulations, the two rivers were represented in the Model using "custom conduits". The conduits' cross-sectional geometry and physical parameters (i.e., Manning's n) were imported from the existing Hydrologic Engineering Centers River Analysis System (HECRAS) model of the two rivers developed by University of New Hampshire (UNH) as part of the CAPE project.

Precipitation and Boundary Conditions

To simulate runoff, the Model was run using the 10-yr, 24-hr design storm. The design storm distribution was obtained from Hydrological Simulation Program-Fortran (HSPF), as shown in Figure 2 below. This unitless design storm distribution was scaled up according to the total estimated storm event depth for each scenario. The storm event depths were 4.72", 5.29", and 5.66" for current (2010), 2040, and 2070 scenarios, respectively. The increased storm event depth for 2040 and 2070 is intended to reflect the projected levels of precipitation increase due to climate change. Storm event depths were provided by Dr. Paul Kirshen at UNH as part of the CAPE project.

As part of the CAPE project, a Hydrologic Engineering Center Hydrologic Modeling System (HEC-HMS) model of the entire Exeter-Squamscott watershed was developed by UNH to quantify hydrological conditions for 2010, 2040 and 2070. The 10-yr, 24-hr storm peak flow rates at Pickpocket Dam and Little River, as predicted by the HEC-HMS model, were entered as constant flow rates into the Model at the upstream boundary junctions representing the Pickpocket Dam and the headwaters of Little River.

The downstream boundary is the water surface elevation of the tidal portion of the Squamscott River at its intersection with Wheelwright Creek. Depending on the modelled scenario, this water surface elevation either represented a typical tidal elevation (Mean Higher-High Water), or the 100-year coastal storm surge elevation. In either case, the boundary condition was maintained at a static elevation for the

duration of each model run. Table 1 summarizes the precipitation data and boundary conditions for the five model scenarios performed in this analysis.

Model Calibration²

The Model was calibrated using flow records for the storm sewered areas and the HEC-HMS model for the non-sewered areas.

For the sewered areas of Exeter, flow records were obtained from a pressure transducer at a catch basin located at the intersection of Park Street and Water Street in Exeter, during June and July of 20131. Observed flows at this catch basin were compared to modeled flows, and this comparison was used for calibration. Sewershed drainage area parameters were adjusted in an iterative process to maximize Nash-Sutcliffe efficiency (E) and minimize the difference in runoff volume during four monitored precipitation events. The final set of calibration parameters caused the model to perform with a Nash-Sutcliffe efficiency E = 0.352 and a runoff volume difference of -5.3%.

For the non-sewered areas, the HEC-HMS model results were used to calibrate the Model. Based on the calibration, the two models appear to be in modest agreement.

Modification of CAPE Model for the Lincoln Street Watershed Analysis

This section describes the modifications made to the existing CAPE Model in order to apply it to the Lincoln Street Watershed Analysis. This analysis focused in on a small portion of the modeled area from the CAPE Model. Consequently, it was necessary to downsize the CAPE Model and also add resolution at certain points within the drainage network. Ultimately, representations of BMPs 1, 2, 3, and 5 were added to the model, along with additional sewer system infrastructure necessary to divert flows at the level desired. Once all of the CAPE Model components were adjusted to a satisfactory degree, PCSWMM was used to run a 2D simulation to determine flooding extent during the 10-year, 24-hour storm event.

Down-sizing of Drainage Network

The CAPE Model covers a much larger area than the focus area for this effort. Consequently, the decision was made to remove all model components outside of the S10 watershed because these features had no impact on the hydrologic or hydraulic dynamics within the Lincoln Street watershed.

Adjustments to the Drainage Network

After downsizing the drainage network to represent only the S10 watershed, it was necessary to add resolution in certain areas and adjust certain model parameters so that the model would suit the analytical needs of this effort. These adjustments were:

- Updating invert elevations for catch basins and manholes in the vicinity of the proposed locations for BMPs 1, 2, 3, and 5.
- Updating pipe diameters in the vicinity of the proposed BMP sites.
- Adding nodes representing catch basins and manholes in areas around the proposed BMP sites.

² Methodology and results are summarized in the memorandum prepared by Geosyntec Consultants, dated 31 October 2013, entitled "CAPE: Storm sewershed runoff model calibration."

• Subdivision of Existing Model Subcatchments for BMPs 3.1-3.6, 3.8, 3.9, and 3.20-3.22. A topographic analysis was used to determine the drainage areas for these BMPs, and these drainage areas were re-directed to the BMPs rather than directly into the drainage network.

Addition of BMPs 1, 2, 3, and 5 to CAPE Model

Once the necessary adjustments to the drainage network were made, the final suite of BMPs (1, 2, 3.1-3.6, 3.8, 3.9, 3.20-3.22, and 5) were added to the PCSWMM model. All BMP designs were originally generated using HydroCAD, a modeling package which is more capable of capturing structural details that are integral to the hydraulic function of a BMP. In transferring the BMP designs from HydroCAD to PCSWMM, modifications were made to preserve the HydroCAD-predicted function. The main difference being that PCSWMM is not capable of representing void space in a storage unit, requiring the modeling team to decrease the heights of each BMP by 40% to account for the stone fill. This allowed for the preservation of surface areas which are more important for exfiltration rates and overall BMP function. For BMPs 3.1-3.22, the PCSWMM-modeled surface areas were further adjusted until the desired performance for the ¹/₂" sized units was achieved:

Overflow = 0cfs during the 0.5" storm Overflow > 0cfs during the 0.6" storm

It is important to note that final designs for BMPs 1, 2, 3, and 5 were derived from a HydroCAD modeling effort, not from the use of SWMM. HydroCAD is more capable of capturing the design details of stormwater BMPs. However, the SWMM model was used to determine the hydrologic impacts of the BMPs on the S10 watershed.

PCSWMM 2D Simulation

As a final modeling step, PCSWMM was used to determine the flooding extent during the 10-year, 24-hour storm event with and without the recommended suite of BMPs. This involved tying the 1-D SWMM model in with LiDAR data (LiDAR for the Northeast, 2011), a process which is supported by a PCSWMM 2-D modeling tool.



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Memorandum

Date:31 October 2013To:Paul Kirshen, University of New HampshireFrom:Robert Roseen, Geosyntec Consultants
Renee Bourdeau, Geosyntec Consultants
Chad Yaindl, Geosyntec ConsultantsSubject:CAPE: Storm sewershed runoff model calibration

SUMMARY

This memorandum describes the methods and results of the model calibration effort for the Exeter storm sewer model. Flow records were obtained from a pressure transducer at catch basin CB534, located at the intersection of Park Street and Water Street, during June and July of 2013. Observed flows at CB534 were compared to modeled flows in conduit C34 (which is the outlet of CB534). Sewershed parameters were adjusted in an iterative process to maximize Nash-Sutcliffe efficiency (E) and minimize the difference in runoff volume during four precipitation events. The final set of calibration parameters caused the model to perform with an efficiency E = 0.352 and a runoff volume difference of -5.3%.

CALCULATION OF MONITORED FLOWRATE

Monitoring data at catch basin CB534 was collected using a pressure transducer to collect a 5minute time series of absolute pressure and temperature. Barometric pressure and precipitation records were obtained a weather station located in Stratham, New Hampshire. Absolute pressure at CB534 was converted to water depth above the transducer using the barometric pressure record. Using the water depth above the transducer, a water depth above the outlet pipe invert was calculated by subtracting the known offset between the transducer and the pipe invert.

Flow at CB534 was calculated assuming the outlet pipe was inlet controlled and that the water depth measured by the transducer reflected headwater above the pipe invert. To calculate observed flow the following equations were used:

$$\frac{HW}{d} = \frac{E_c}{d} + K \left[\frac{Q}{Ad^{0.5}}\right]^M - 0.5S; (Inlet unsubmerged)$$

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$$\frac{HW}{d} = c \left[\frac{Q}{Ad^{0.5}}\right]^2 + Y - 0.5S; (Inlet submerged)$$

where, HW is head above the culvert inlet, E_c is the minimum specific energy, d is the diameter of the pipe, Q is the discharge, A is the full cross-sectional area of the barrel, S is the pipe slope, and K, M, c, and Y are constants reflecting various types of inlet configurations.

CHOICE OF PRECIPITATION EVENTS

During the observed period of record (June through July 2013), the modeled flowrates at conduit C34 were compared to observed flowrates at CB 534. Four precipitation events were chosen for calibration based on a qualitative process. The qualitative process included determining if a precipitation event produced a modeled runoff hydrograph with approximately the same shape and magnitude as the observed hydrograph. In several instances, the model produced a large peak event where no such event was evident in the monitoring record. These discrepancies are most likely due to potential differences in precipitation intensity between location of the CB 534 watershed and the Stratham precipitation gage and less likely a function of watershed parameters.

CALIBRATION OF SUBWATERSHED PARAMETERS

Presented in Table 1, are the subwatershed parameters used in the Exeter storm sewereshed model and whether these parameters are unique to each subcatchment if they were calculated using GIS processes or if an estimated model wide value was used (default).

The subwatershed parameters were considered for calibration, primarily the default values. Using an iterative process, the watershed parameters were adjusted to minimize the difference in runoff volume between the observed and modeled during the four calibration precipitation events. To determine the effectiveness of the calibration, the Nash-Sutcliffe efficiency (E) was used to assess the predictive power of the hydrologic model. The efficiencies range from negative infinity (- ∞ to 1), with an efficiency of 1 corresponding to a perfect match between observed and modeled. For each of the four calibration events, Nash-Sutcliffe efficiency and observed and modeled runoff volumes were calculated. The subwatershed model parameters were adjusted to provide the highest efficiency and the lowest percent difference between observed and modeled runoff volumes. Results of the two calibration indicators are presented in Table 2 and hydrographs for the four events presented as Figure 1. The calibration process increased efficiency (E) from 0.291 to 0.352, and reduced difference in runoff volume by approximately 5%. To achieve this, the following subwatershed parameters were adjusted, which are also presented in Table 1:

- Increase of Manning's n for pervious surfaces;
- Increase of storage depth for both impervious and pervious surfaces;
- Routing of pervious surface runoff onto impervious surfaces (i.e. lawn runoff onto driveway/road);
- Increase of calculated curve number by 7%; and
- Decrease in the soil drying time from 4 to 2 days.

Subwatershed Parameter	Unique (calculated) or Default Value [U or D]	Default Value	Post- calibration Value
Area	U		
Width	U		
% Slope	U		
% Impervious	U		
N-Impervious	D	0.01	0.01
N-Pervious	D	0.1	0.15
Dstore Impervious	D	0.05	0.012
Dstore Pervious	D	0.05	0.18
%Zero Impervious	D	25	25
Subarea Routing	D	OUTLET	IMPERVIOUS
Percent Routed	D	100	100
Infiltration Curve Number	U		x1.07
Soil Drying Time	D	4 days	2 days

Table 1. Subwatershed Parameters Pre- and Post-calibration

Table 2. Calibration indicators

PRE-CALIB	RATION		POST-CALIBRATION			
Event	E	Volume % Diff.	Event	E	Volume % Diff.	
6/7/2013 0:00	0.283	60%	6/7/2013 0:00	0.499	10%	
6/10/2013 12:00	0.538	-33%	6/10/2013 12:00	-0.072	21%	
6/11/2013 18:00	0.037	-63%	6/11/2013 18:00	0.452	-45%	
7/1/2013 12:00	0.307	-5%	7/1/2013 12:00	0.528	-7%	
Average	0.291	-10%	Average	0.352	-5.3%	



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Figure 1. Four calibration events, monitored and modeled flowrates, location CB 534.

APPENDIX E: POLLUTANT LOAD METHODOLOGY

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Pollutant Loading and BMP Costing Analysis

A planning level pollutant loading and BMP costing analysis was performed for each of the 7 potential BMPs identified for the Lincoln Street watershed. The soil type, BMP type, and land use type for each BMP is shown in Table 1 - BMP type, soil, and land use summary. These were used in conjunction with performance curves from the WISE, 2015¹ analysis to determine expected runoff and nitrogen load reductions associated with each BMP.

These curves and associated pollutant load reduction estimates are shown in Section C.1, below.

Estimates for the cost per acre of drainage area for each BMP type from the WISE, 2015¹ analysis were used to estimate the total and unit costs associated with the nitrogen load reductions for each BMP. The numbers used for these estimates are shown in Section C.2, below.

BMP Location	Soil Type	Proposed BMP Type
1	А	Subsurface Infiltration
2	А	Subsurface Infiltration
3.1	А	Bioretention
3.2	А	Bioretention
3.3 - 3.6	А	Bioretention
4	А	Subsurface infiltration
5	А	Subsurface infiltration
6	С	Bioretention
7	А	Subsurface Infiltration

Table 1 - BMP type, soil, and land use summary

¹ Roseen, R., Watts, A., Bourdeau, R., Stacey, P., Sinnott, C., Walker, T., Thompson, D., Roberts, E., and Miller, S. (2015). Water Integration for Squamscott Exeter (WISE), Preliminary Integrated Plan, Final Technical Report. Portsmouth, NH, Geosyntec Consultants, University of New Hampshire, Rockingham Planning Commission, Great Bay National Estuarine Research Reserve, Consensus Building Institute.

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C.1 Pollutant Loading Analysis

Pollutant Loading Calculation Example

The following example and accompanying figures explain the approach taken for the pollutant loading and volume reduction analysis performed in this study with a BMP of the following characteristics:

- subsurface infiltration system,
- 1" water quality volume,
- type B soil,
- commercial land use,

From the BMP performance curve for a subsurface infiltration system pollutant removal and volume reduction are determined as follows:

- 1. **Determine initial load.** Where the BMP curve for nitrogen (black curves) crosses the left hand vertical axis (capture depth=0) determine the initial TN load based on commercial land use = 13.3 lbs/ac/yr.
- 2. **Determine treated load.** Locate performance curve for soil type B for the capture volume. A system treating a 1" water quality volume for 1 acre will have a treated load of 2.3 lbs/ac/yr.

Example 1: BMP optimization for pollutant load with subsurface infiltration at 1" water quality volume



3. **Determine load removed.** An initial load of 13.3 lbs/ac/yr and a treated load of 2.3 lbs/ac/yr removes 11 lbs/ac/yr or 83% annual TN reduction.

 $\frac{\text{Treated Load}}{\text{Initial Load}} = \frac{11}{13.3} = 83\% \text{ TN reduction annually}$

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- 4. **Determine initial runoff volume.** Where the BMP curve for volume (blue curves) crosses the left hand vertical axis (capture depth=0) determine the initial runoff volume based on the right hand axis for commercial land use = 0.9 million gallons/ac/yr.
- 5. **Determine treated runoff volume.** Locate performance curve for soil type B for the capture volume. A system treating a 1" water quality volume for 1 acre will have a runoff volume = 0.11 million gallons/ac/yr.

Example 2: BMP optimization for volume with subsurface infiltration at 1" water quality volume



6. **Determine volume removed.** An initial runoff volume of 0.9 MG/ac/yr and a treated runoff volume of 0.11 MG/ac/yr removes 0.79 MG/ac/yr or 88% annual runoff reduction.

 $\frac{\text{Treated Runoff Volume}}{\text{Initial Runoff Volume}} = \frac{0.11}{0.9} = 88\% \text{ runoff volume reduction annually}$

The complete methods can be found in the BMP Decision Support System (BMPDSS)(EPA 2010)² and WISE Project (Roseen et al 2015)¹. This approach was developed in cooperation with EPA Region 1 to support an Integrated Planning and Permitting framework for watershed scale nitrogen management for the Exeter-Squamscott Watershed.

² EPA and I. Tetra Tech (2010). Stormwater Best Management Practices (BMP) Performance Analysis. United States Environmental Protection Agency – Region 1, Boston, MA.

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The following tables display the actual numbers used to calculate pollutant load reductions in this analysis, applying the methodology outlined above in Examples 1 and 2. The associated BMP performance curves can be found in WISE, 2015¹, pages 92-180.

Table 2 - Performance estimates for BMP 6

вмр	Drainage Area (acres)	Annual N Load (lbs)	1/4" Volume Reduction (ft ³)	1/2" Volume Reduction (ft ³)	1/4" N Reduction (lbs)	1/2" N Reduction (lbs)
6	1.73	27.27	1,569	3,138	5	6

Table 3 - Performance estimates for BMP 3

вмр	Drainage Area (acres)	Annual N Load (lbs)	1/4" Volume Reduction (ft ³)	1/2" Volume Reduction (ft ³)	1/4" N Reduction (lbs)	1/2" N Reduction (lbs)
3	12.33	104.64	11,192	22,384	65	84

Table 4 - Performance estimates for BMPs 1, 2, 4, 5, and 7

вмр	Drainage Area (acres)	Annual N Load (lbs)	1/4" Volume Reduction (ft ³)	1/4" Volume 1/2" Volume Reduction (ft ³) Reduction (ft ³)		1/2" N Reduction (lbs)
1	11.15	76.6	10,116	20,232	42	62
2	24.56	157.6	22,291	44,582	84	120
4	38.63	252.2	35,059	70,119	114	174
5	17.85	113.7	16,199	32,397	59	86
7	24.79	152.3	22,498	44,997	77	113

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C.2 COSTING ANALYSIS



The WISE, 2015³ study developed estimates for the cost of sizing a variety of stormwater capture systems to manage different size storm events. Table 5 - BMP cost estimates developed for WISE, 2015 shows the estimated per-acre costs for bioretention and subsurface infiltration systems designed to manage the 0.25" and 0.5" storm events.

In order to calculate the total cost of a BMP using this table, it is necessary to multiply the drainage area by the cost shown in Table 5 - BMP cost estimates developed for WISE, 2015. The unit cost (\$ per pound of nutrient load reduction) can then be derived by dividing the total cost by the total expected annual nutrient load reduction.

Table 5 - BMP cost estimates developed for WISE, 2015

	Capitol Cost Range Based on Capture Depth of 1-acre drainage area (\$)							
Structural Treatment Practice		0.25 in.	0.5 in.					
	LOW	HIGH	FINAL	LOW	HIGH	FINAL		
Bioretention with Underdrain (No Pretreatment) ¹	\$2,759	\$40,000	\$11,400	\$5,518	\$60,000	\$18,300		
Subsurface Infiltration	\$18,000	\$35,000	\$18,500	\$25,000	\$45,000	\$28,000		

1. Pretreatment not required for direct runoff from impervious surfaces (i.e., roof tops and parking lots).

³ Roseen, R., Watts, A., Bourdeau, R., Stacey, P., Sinnott, C., Walker, T., Thompson, D., Roberts, E., and Miller, S. (2015). Water Integration for Squamscott Exeter (WISE), Preliminary Integrated Plan, Final Technical Report. Portsmouth, NH, Geosyntec Consultants, University of New Hampshire, Rockingham Planning Commission, Great Bay National Estuarine Research Reserve, Consensus Building Institute.

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BMP Cost Calculation Example

The following example explains the approach taken for the costing analysis performed in this study using BMP 1, which has the following relevant characteristics:

- subsurface infiltration system,
- 0.25" water quality volume,
- 11.1 acre drainage area
- 42 lbs annual Nitrogen load reduction when sized for 0.25" water quality volume (from Pollutant Loading Analysis)

1. Reference Table 5 to determine the capital cost per-acre for a subsurface infiltration system sized to capture the 0.25" water quality volume. For this analysis, we use the 'Final' estimate rather than the 'High' or 'Low' estimates, yielding a per-acre cost of \$18,500.

2. Multiply the per-acre cost by the BMP drainage area. For BMP 1, the drainage area is 11.1 acres: [11.15 acres] x [\$18,500 / acre] = \$206,221

3. Divide the total cost from Step 2 by the annual Nitrogen Load reduction potential to derive the unit cost for the BMP:

Table 6 – Lincoln Street costing analysis results, shows the results of this analysis applied to the Lincoln Street watershed.

		1/4" WQ	1/4" WQV System		System
BMP Location	Drainage Area (acres)	Total Cost	Unit Cost (\$/lb)	Total Cost	Unit Cost (\$/lb)
1	11.1	\$206,221	\$4,900	\$312,118	\$5,000
2	24.6	\$454,414	\$5 <i>,</i> 400	\$687,761	\$5,700
3.1	6.9	\$78,509	\$2,200	\$126,028	\$2,700
3.2	4.2	\$47,512	\$2,500	\$76,270	\$3,100
3.3 - 3.6	1.3	\$14,569	\$1,400	\$23,388	\$1,800
4	38.6	\$714,710	\$6,300	\$1,081,724	\$6,200
5	17.9	\$330,222	\$5,600	\$499,796	\$5,800
6	1.7	\$19,713	\$3,800	\$31,644	\$5,000
7	24.8	\$458,646	\$5,900	\$694,167	\$6,100

Table 6 – Lincoln St	reet costing	analysis results
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APPENDIX F: OUTREACH EFFORTS







REGIONAL CONTEXT

- In 2009, NHDES concluded that many sub-estuaries in the Great Bay Estuary were impaired by nitrogen, and the Great Bay was placed on the Clean Water Act (CWA) Sec. 303(d) list of impaired and threatened waters (NHDES, 2009).
- New and revised discharge permits in the watershed are now subject to additional nitrogen requirements including the National Pollutant Discharge Elimination System (NPDES) permits for wastewater treatment facilities, and Municipal Separate Storm Sewer Discharge (MS4) permits for stormwater.



WASTEWATER & MS4 BACKGROUND

- In 2012 EPA issued a new wastewater permit with a total nitrogen effluent limit of 3 mg/l.
- Negotiated an Administrative Order on Consent (AOC) to allow a staged approach.
- AOC requires a Nitrogen Control Plan by September 30, 2018 with a schedule for implementing specific nitrogen control measures.
- 2017 NH Small MS4 issued, effective in 2018, includes significant new elements such as a focus on illicit discharge detection and elimination, and nutrient management through BMP retrofits.



PROJECT OVERVIEW

OBJECTIVES

- Build upon the WISE analysis to identify specific green infrastructure (GI) and low impact development (LID) practices that can be installed in Exeter to manage stormwater, reduce nutrient loads, and increase resiliency.
- 2. Design green infrastructure (GI) practices within the watershed to help reduce the risk of flooding while reducing pollutant load into the Squamscott River.

- OUTCOMES 1. Identify a suite of BMPs that will reduce nutrient loading and flooding.
- 2. Provide performance metrics for BMPs in terms of total costs, unit costs (\$/lb N $\,$ reduced), and flood mapping for volume and the duration.
- Develop GI concepts and final designs that can be used for bidding and construction for 3. the future Lincoln Street CIP planned for FY18.

TASKS

- 1. Watershed Modeling
- 2. Potential Green Infrastructure **Retrofit Locations**
- 3. Project Design
- 4. Other Locations for BMPs
- 5. Nutrient and Flooding Reduction May 9, 2017





2









				NITRO	OGEN	I LOADI	NG RED	DUCTIO	N POTEN	TIAL	- -		
	BMP #	BMP Type BMP #	Draina	age Arelaittikhälykke	Soil Bythen ah Spo	tageitindeğiler Eşipe Anna	i Dialoag (iks) a (acres)	Annual TN Load (lbs)	Annual N Load Reduction Potential (Ibs)	\$/LBS NITROGEN	d Reduc asign Co ial (lbs)	ion t Estimate S/LBS/nnual N Load Reduction NITROGEN Potential (lbs)	\$/L85 NTROEN
INTER STREET		WINTER STREET		WINTER STREET	1	Subsurface Infiltration	12.88	90.7	68.2	\$675]]		
					2	Subsurface Infiltration	24.56	157.6	120.2	\$610	J		
					Total		37.44	248.3	188.4				
	BMP #	BMP Type BMP #	Draina	age Arelaillishiðjýdae	Soil B ypenin Syn	tageländettete	i Dizinag(iks) a (acres)	Annual TN Load (Ibs)	Annual N Load Reduction Potential (lbs)	\$/LBS NITROGEN	d Reduc asign Co ial (lbs)	ion S/LB\$nnual N Load Reduction NITROGEN Potential (lbs)	S/LBS NITROEN
					3.1	Tree Planter	0.20	2.5	2.0	\$3,924	וכ		
					3.2	Tree Planter	0.13	1.7	1.3	\$5,031	ונ		
					3.3	Tree Planter	0.27	3.4	2.6	\$4,276	1 1		
COLN STREET		LINCOLN STREET		LINCOLN STREET	3.4	Tree Planter	0.22	2.9	2.2	\$4,459]]		
NORTH		NORTH		NORTH	3.5	ROW Infiltration- Grassed	0.24	2.4	1.8	\$3,621]]		
					3.6	ROW Infiltration- Grassed	0.78	7.2	5.7	\$3,812	J		
					3.8	ROW Infiltration- Grassed	1.20	9.1	7.1	\$3,060	J		
					3.9	ROW Infiltration- Grassed	0.70	5.6	4.2	\$3,233	J		
					3.22	ROW Infiltration- Grassed	0.20	1.3	1.0	\$2,716			
					Total		3.94	36.2	27.9				
											- I		
	BMP #	BMP Type BMP #	Draina	age Arelanshillydee	Soil B /Mah h Sya	agelandetesje Annu	Dizioagéiks èa (acres)	Annual TN Load (Ibs)	Annual N Load Reduction	\$/LBS	d Reduc	t Estimate S/LBS/nnual N Load Reduction	\$/LBS
COLN STREET		LINCOLN STREET		LINCOLN STREET					Potential (Ibs)	NITROGEN	iai (ibs)	NITRUGEN Potential (Ibs)	NITROGEN
SOUTH		SOUTH		SOUTH	3.20	RUW Infiltration- Grassed	1.60	13.9	10.7	\$3,046	- 1		
					3.21 Tetal	KUW Inhibration- Grassed	0.24	1.4	1.0	\$2,/16	-		
				-	TOLAI		1.04	13.3	11.7				
									Annual N Load Reduction	\$/IRS	d Beduc	ion S/IBSonual N Load Reduction	\$/J #5
RONT STREET	BMP #	FRONT STREET BMP #	Draina	FRONT STREET	Soil BARANA Agen	agelanzēļātrēsipe Anna:	a Dialoagélikska (acres)	Annual TN Load (lbs)	Potential (lbs)	NITROGEN	asign Co ial (lbs)	t Estimate NITROGEN Potential (lbs)	NTROGEN
					5	Subsurface Infiltration	20.29	. 138.3	71.7	\$585	1		
			5	5/5/2017		197	ay 5, 2017 Con Conn	rresentation			7	1	
				TOTAL			63.51	438	299.7		ו כ		
			_										































WASTEWATER & MS4 BACKGROUND

- In 2012 EPA issued a new wastewater permit with a total nitrogen effluent limit of 3 mg/l.
- Negotiated an Administrative Order on Consent (AOC) to allow a staged approach.
- AOC requires a Nitrogen Control Plan by September 30, 2018 with a schedule for implementing specific nitrogen control measures.
- 2017 NH Small MS4 issued, effective in 2018, includes significant new elements such as a focus on illicit discharge detection and elimination, and nutrient management through BMP retrofits.









LOW IMPACT DEVELOPMENT





































n	50/	co		N 4 ATEC					
55/0 CUST ESTIIVIATES									
,	WINTER	BMP #	Drainage Area (acres)	Annual TN Reduction (Ibs)	% Load Reduction	95% Design Cost Estimate	\$/LBS NITROGEN		
	STREET	1	12.9	68.2	76%	\$45,900	\$680		
		2	24.6	120.2	76%	\$79,000	\$660		
5	Subtotal	-	37.4	188.4	76%	\$124,900			
		BMP #	Drainage Area (acres)	Annual TN Reduction (lbs)	% Load Reduction	95% Design Cost Estimate	\$/LBS NITROGEN		
		3.1	0.2	2.0	80%	\$8,000	\$4,000		
		3.2	0.1	1.3	76%	\$6,600	\$5,080		
1	LINCOLN	3.3	0.3	2.6	77%	\$12,000	\$4,620		
	STREET	3.4	0.2	2.2	77%	\$9,900	\$4,500		
	NORTH	3.5	0.2	1.8	75%	\$7,000	\$3,890		
		3.6	0.8	5.7	79%	\$21,800	\$3,830		
		3.8	1.2	7.1	78%	\$22,000	\$3,100		
		3.9	0.7	4.2	75%	\$13,600	\$3,240		
		3.22	0.2	1.0	77%	\$3,000	\$3,000		
5	Subtotal	-	3.9	27.9	77%	\$103,900	-		
ı		BMP #	Drainage Area (acres)	Annual TN Reduction (Ibs)	% Load Reduction	95% Design Cost Estimate	\$/LBS NITROGEN		
	SOUTH	3.20	1.6	10.7	77%	\$33,000	\$3,090		
		3.21	0.2	1.0	72%	\$2,800	\$2,800		
	Subtotal	-	1.8	11.7	76%	\$35,800	-		
	FRONT	BMP #	Drainage Area (acres)	Annual TN Reduction (Ibs)	% Load Reduction	95% Design Cost Estimate	\$/LBS NITROGEN		
		5	20.3	71.7	52%	\$45,200	\$640		
	Total	-	63.5	299.7	69%	\$309,800	-		



APPENDIX G: ENGINEERING COST ESTIMATES

ENGINEERING DESIGN COSTS PHASE 1: LINCOLN STREET SUBWATERSHED NITROGEN CONTROL STRATEGIES

	BMP #	ВМР Туре	Drainage Area (acres)	Annual TN Load (lbs)	Engineering Cost Estimate	Annual N Load Reduction Potential (lbs)	\$/LBS NITROGEN
WINTER STREET	1	Subsurface Infiltration	12.88	90.7	\$45,900	68.2	\$675
	2	Subsurface Infiltration	24.56	157.6	\$78,700	120.2	\$656
	Total	-	37.44	248.3	\$124,600	188.4	-

	BMP #	ВМР Туре	Drainage Area (acres)	Annual TN Load (lbs)	Engineering Cost Estimate	Annual N Load Reduction Potential (lbs)	\$/LBS NITROGEN
	3.1	Tree Planter	0.20	2.5	\$7,848	2.0	\$3,924
	3.2	Tree Planter	0.13	1.7	\$6,540	1.3	\$5,031
	3.3	Tree Planter	0.27	3.4	\$11,118	2.6	\$4,276
LINCOLN STREET	3.4	Tree Planter	0.22	2.9	\$9,810	2.2	\$4,459
NORTH	3.5	ROW Infiltration- Grassed	0.24	2.4	\$6,518	1.8	\$3,621
	3.6	ROW Infiltration- Grassed	0.78	7.2	\$21,728	5.7	\$3,812
	3.8	ROW Infiltration- Grassed	1.20	9.1	\$21,728	7.1	\$3,060
	3.9	ROW Infiltration- Grassed	0.70	5.6	\$13,580	4.2	\$3,233
	3.22	ROW Infiltration- Grassed	0.20	1.3	\$2,716	1.0	\$2,716
	Total	-	3.94	36.2	\$101,586	27.9	-

LINCOLN STREET SOUTH	BMP #	ВМР Туре	Drainage Area (acres)	Annual TN Load (lbs)	Engineering Cost Estimate	Annual N Load Reduction Potential (lbs)	\$/LBS NITROGEN
	3.20	ROW Infiltration- Grassed	1.60	13.9	\$32,591	10.7	\$3,046
	3.21	ROW Infiltration- Grassed	0.24	1.4	\$2,716	1.0	\$2,716
	Total	-	1.84	15.3	\$35,307	11.7	-

FRONT STREET	BMP #	ВМР Туре	Drainage Area (acres)	Annual TN Load (lbs)	Engineering Cost Estimate	Annual N Load Reduction Potential (lbs)	\$/LBS NITROGEN
	5	Subsurface Infiltration	20.29	138.3	\$45,200	71.7	\$630.40

TOTAL 63.51 438 \$306,694 299.7 -						4000.000		
	TOTAL	-	-	63.51	438	\$306,694	299.7	-

BMP-1

Costcode	Description	Quantity	Column1	Material	Labor	Other	Total
			Unit	\$	\$	\$	\$
General							
01410	TESTING	1.00		0.00	0.00	0.00	0.00
014101100	Aggregate Infiltration test	2.00	Ea	0.00	270.00	262.50	532.50
015004230	Board-up cover, two sheets plywood	1.00	Ea	51.21	100.63	0.00	151.84
01600	EQUIPMENT RENTAL	1.00		0.00	0.00	0.00	0.00
016001080	Backhoe, diesel, crawler, 1 Cy	3.00	Day	0.00	2,760.00	4,181.25	6,941.25
016001360	Core drill, electric, 2-1/2 HP	1.00	Day	0.00	0.00	88.00	88.00
016001720	Edger, lawn, gas	1.00	Day	0.00	0.00	35.00	35.00
016002660	Saw, concrete, gas	1.00	Day	0.00	0.00	110.00	110.00
016002940	Transit tripod set	1.00	Day	0.00	0.00	53.75	53.75
016003020	Truck, dump, tandem, 12 T load	3.00	Day	0.00	0.00	1,530.00	1,530.00
017001100	Final cleanup	1540.00	Sf	0.00	0.00	1,925.00	1,925.00
	Subtotal Genera	I		51.21	3,130.63	8,185.50	11,367.34
Sitework							
02050	DEMOLITION	1.00		0.00	0.00	0.00	0.00
020502130	Saw cutting, paving	56.00	Lf	0.00	77.84	25.20	103.04
020502140	Saw cutting, concrete	8.00	Lf	0.00	264.53	5.60	270.13
02060	AGGREGATE AND SOILS	1.00		0.00	0.00	0.00	0.00
020601130	Crushed Stone, Drainage, 1/2"	214.00	Су	5,082.50	0.00	0.00	5,082.50
02070	GEOSYNTHETICS	1.00		0.00	0.00	0.00	0.00
020701110	Geotextiles- Mirafi 160N	675.00	Sf	263.25	0.00	0.00	263.25
02100	SITE PREPARATION	1.00		0.00	0.00	0.00	0.00
021001390	Test Pits	1.00		0.00	0.00	0.00	0.00
02200	EARTHWORK	1.00		0.00	0.00	0.00	0.00
022001010	General excavation	467.00	Су	0.00	4,315.08	2,685.25	7,000.33
022003330	Area backfill, 7' deep	1400.00	Sf	0.00	700.00	490.00	1,190.00
02370	EROSION AND SEDIMENTATION CONTROL	1.00		0.00	0.00	0.00	0.00
023701020	3' Silt fence and haybales	300.00	Lf	825.00	0.00	0.00	825.00
02500	PAVING AND SURFACING	1.00		0.00	0.00	0.00	0.00
025001110	Grade and compact	18.00	Sy	0.00	82.80	46.80	129.60
025002160	Asphalt paving repair	18.00	Sy	290.70	331.20	189.00	810.90
02600	DRAINAGE	1.00		0.00	0.00	0.00	0.00
026001630	Drainage pipe, HDPE, 12" dia	50.00	Lf	855.00	192.50	37.50	1,085.00
026201210	PRETX-Inline, 5' dia, 8' deep	1.00	Ea.	3,325.00	440.00	0.00	3,765.00
026201310	Subsurface chambers 330XL	10.00	Ea.	3,325.00	880.00	0.00	4,205.00
02900	LANDSCAPING	1.00		0.00	0.00	0.00	0.00
029001210	Area prep for seeding	156.00	Sy	0.00	57.72	4.68	62.40
029001220	Place top soil, by hand	156.00	Sy	0.00	430.56	0.00	430.56
029002110	Seeding	156.00	Sy	15.60	57.72	3.12	76.44
	Subtotal Sitework	(13,982.05	7,829.95	3,487.15	25,299.15
	Estimate Tota	1		14,033.26	10,960.58	11,672.65	36,666.49
	Contingency	25.00	%	3,508.32	2,740.15	2,918.16	9,166.62
	Estimate Tota			17,541.58	13,700.73	14,590.81	45,833.11

BMP-2

Costcode	Description	Quantity	Unit	Material	Labor	Other	Total
				\$	\$	\$	\$
General				·		I	
01410	TESTING	1.00		0.00	0.00	0.00	0.00
014101100	Aggregate Infiltration test	2.00	Ea	0.00	270.00	262.50	532.50
015004230	Board-up cover, two sheets plywood	1.00	Ea	51.21	100.63	0.00	151.84
01600	EQUIPMENT RENTAL	1.00		0.00	0.00	0.00	0.00
016001080	Backhoe, diesel, crawler, 1 Cy	3.00	Day	0.00	2,760.00	4,181.25	6,941.25
016001360	Core drill, electric, 2-1/2 HP	1.00	Day	0.00	0.00	88.00	88.00
016001720	Edger, lawn, gas	1.00	Day	0.00	0.00	35.00	35.00
016002660	Saw, concrete, gas	1.00	Day	0.00	0.00	110.00	110.00
016002940	Transit tripod set	1.00	Day	0.00	0.00	53.75	53.75
016003020	Truck, dump, tandem, 12 T load	3.00	Day	0.00	0.00	1,530.00	1,530.00
017001100	Final cleanup	2200.00	Sf	0.00	0.00	2,750.00	2,750.00
	Subtotal General			51.21	3,130.63	9,010.50	12,192.34
Sitework							
02050	DEMOLITION	1.00		0.00	0.00	0.00	0.00
020502130	Saw cutting, paving	56.00	Lf	0.00	77.84	25.20	103.04
020502140	Saw cutting, concrete	8.00	Lf	0.00	264.53	5.60	270.13
02060	AGGREGATE AND SOILS	1.00		0.00	0.00	0.00	0.00
020601130	Crushed Stone, Drainage, 1/2"	202.00	Су	4,797.50	0.00	0.00	4,797.50
02070	GEOSYNTHETICS	1.00		0.00	0.00	0.00	0.00
020701110	Geotextiles- Mirafi 160N	720.00	Sf	280.80	0.00	0.00	280.80
02100	SITE PREPARATION	1.00		0.00	0.00	0.00	0.00
021001390	Test Pits	1.00		0.00	0.00	0.00	0.00
02200	EARTHWORK	1.00		0.00	0.00	0.00	0.00
022001010	General excavation	1037.00	Су	0.00	9,581.88	5,962.75	15,544.63
022003330	Area backfill, 7' deep	2000.00	Sf	0.00	1,000.00	700.00	1,700.00
02370	EROSION AND SEDIMENTATION CONTROL	1.00		0.00	0.00	0.00	0.00
023701020	3' Silt fence and haybales	300.00	Lf	825.00	0.00	0.00	825.00
02500	PAVING AND SURFACING	1.00		0.00	0.00	0.00	0.00
025001110	Grade and compact	18.00	Sy	0.00	82.80	46.80	129.60
025002160	Asphalt paving repair	18.00	Sy	290.70	331.20	189.00	810.90
02600	DRAINAGE	1.00		0.00	0.00	0.00	0.00
026001630	Drainage pipe, HDPE, 12" dia	50.00	Lf	855.00	192.50	37.50	1,085.00
026201210	PRETX-Inline, 5' dia, 8' deep	1.00	Ea.	3,325.00	440.00	0.00	3,765.00
026201310	Subsurface chambers 330XL	49.00	Ea.	16,292.50	4,312.00	0.00	20,604.50
02900	LANDSCAPING	1.00		0.00	0.00	0.00	0.00
029001210	Area prep for seeding	222.00	Sy	0.00	82.14	6.66	88.80
029001220	Place top soil, by hand	222.00	Sy	0.00	612.72	0.00	612.72
029002110	Seeding	222.00	Sy	22.20	82.14	4.44	108.78
	Subtotal Sitework			26,688.70	17,059.75	6,977.95	50,726.40
	Estimate Total			26,739.91	20,190.38	15,988.45	62,918.74
	Contingency	25.00	%	6,684.98	5,047.60	3,997.11	15,729.69
	Estimate Total			33,424.89	25,237.98	19,985.56	78,648.43
BMP-3 ROW Infiltration Grassed (Typical)

Costcode	Description	Quantity	Unit	Material	Labor	Other	Total
				\$	\$	\$	\$
General							
01410	TESTING	1.00		0.00	0.00	0.00	0.00
014101100	Aggregate Infiltration test	1.00	Ea	0.00	135.00	131.25	266.25
015004230	Board-up cover, two sheets plywood	1.00	Ea	51.21	100.63	0.00	151.84
01600	EQUIPMENT RENTAL	1.00		0.00	0.00	0.00	0.00
016001080	Backhoe, diesel, crawler, 1 Cy	2.00	Day	0.00	1,840.00	2,787.50	4,627.50
016001360	Core drill, electric, 2-1/2 HP	1.00	Day	0.00	0.00	88.00	88.00
016002660	Saw, concrete, gas	1.00	Day	0.00	0.00	110.00	110.00
016002940	Transit tripod set	1.00	Day	0.00	0.00	53.75	53.75
016003020	Truck, dump, tandem, 12 T load	2.00	Day	0.00	0.00	1,275.00	1,275.00
017001100	Final cleanup	110.00	Sf	0.00	0.00	137.50	137.50
	Subtotal General			51.21	2,075.63	4,583.00	6,709.84
Sitework							
02050	DEMOLITION	1.00		0.00	0.00	0.00	0.00
020502140	Saw cutting, concrete	8.00	Lf	0.00	264.53	5.60	270.13
02060	AGGREGATE AND SOILS	1.00		0.00	0.00	0.00	0.00
020601130	Crushed Stone, Drainage, 1/2"	26.00	Су	617.50	0.00	0.00	617.50
020601160	Top soil	3.00	Су	79.80	0.00	0.00	79.80
02070	GEOSYNTHETICS	1.00		0.00	0.00	0.00	0.00
020701110	Geotextiles- Mirafi 160N	210.00	Sf	81.90	0.00	0.00	81.90
020701130	PVC Liner	140.00	Sf	68.60	0.00	0.00	68.60
02100	SITE PREPARATION	1.00		0.00	0.00	0.00	0.00
021001390	Test Pits	1.00		0.00	0.00	0.00	0.00
02200	EARTHWORK	1.00		0.00	0.00	0.00	0.00
022001010	General excavation	26.00	Су	0.00	240.24	149.50	389.74
022003330	Area backfill, 7' deep	100.00	Sf	0.00	50.00	35.00	85.00
02370	EROSION AND SEDIMENTATION CONTROL	1.00		0.00	0.00	0.00	0.00
023701020	3' Silt fence and haybales	70.00	Lf	192.50	0.00	0.00	192.50
02600	DRAINAGE	1.00		0.00	0.00	0.00	0.00
026201610	ROW Infiltration catch basin insert	1.00	Ea.	1,995.00	330.00	0.00	2,325.00
02900	LANDSCAPING	1.00		0.00	0.00	0.00	0.00
029001210	Area prep for seeding	12.00	Sy	0.00	4.44	0.36	4.80
029001220	Place top soil, by hand	12.00	Sy	0.00	33.12	0.00	33.12
029002110	Seeding	12.00	Sy	1.20	4.44	0.24	5.88
	Subtotal Sitework			3,036.50	926.77	190.70	4,153.97
	Estimate Total			3,087.71	3,002.40	4,773.70	10,863.81

BMP-3 Tree Planter (Typical)

Costcode	Description	Quantity	Unit	Material	Labor	Other	Total	
				\$	\$	\$	\$	
General								
01410	TESTING	1.00		0.00	0.00	0.00	0.00	
014101100	Aggregate Infiltration test	1.00	Ea	0.00	135.00	131.25	266.25	
015004230	Board-up cover, two sheets plywood	1.00	Ea	51.21	100.63	0.00	151.84	
01600	EQUIPMENT RENTAL	1.00		0.00	0.00	0.00	0.00	
016001080	Backhoe, diesel, crawler, 1 Cy	2.00	Day	0.00	1,840.00	2,787.50	4,627.50	
016002660	Saw, concrete, gas	1.00	Day	0.00	0.00	110.00	110.00	
016002940	Transit tripod set	1.00	Day	0.00	0.00	53.75	53.75	
016003020	Truck, dump, tandem, 12 T load	2.00	Day	0.00	0.00	1,275.00	1,275.00	
017001100	Final cleanup	110.00	Sf	0.00	0.00	137.50	137.50	
	Subtotal General			51.21	2,075.63	4,495.00	6,621.84	
Sitework								
02050	DEMOLITION	1.00		0.00	0.00	0.00	0.00	
020501320	Flooring demolition, ceramic tile	1.00	Sf	0.00	1.32	0.35	1.67	
020502140	Saw cutting, concrete	8.00	Lf	0.00	264.53	5.60	270.13	
02060	AGGREGATE AND SOILS	1.00		0.00	0.00	0.00	0.00	
020601130	Crushed Stone, Drainage, 1/2"	19.00	Су	451.25	0.00	0.00	451.25	
020601170	Bioretention soil mix	4.00	Су	171.00	0.00	0.00	171.00	
02070	GEOSYNTHETICS	1.00		0.00	0.00	0.00	0.00	
020701110	Geotextiles- Mirafi 160N	210.00	Sf	81.90	0.00	0.00	81.90	
020701130	PVC Liner	140.00	Sf	68.60	0.00	0.00	68.60	
02100	SITE PREPARATION	1.00		0.00	0.00	0.00	0.00	
021001390	Test Pits	1.00		0.00	0.00	0.00	0.00	
02200	EARTHWORK	1.00		0.00	0.00	0.00	0.00	
022001010	General excavation	26.00	Су	0.00	240.24	149.50	389.74	
022003230	Area backfill, 3' deep	40.00	Sf	0.00	9.20	2.80	12.00	
022003330	Area backfill, 7' deep	100.00	Sf	0.00	50.00	35.00	85.00	
02370	EROSION AND SEDIMENTATION CONTROL	1.00		0.00	0.00	0.00	0.00	
023701020	3' Silt fence and haybales	70.00	Lf	192.50	0.00	0.00	192.50	
02500	PAVING AND SURFACING	1.00		0.00	0.00	0.00	0.00	
025004110	Walkways, concrete, 4 in thick, basic	100.00	Sf	143.00	115.00	5.00	263.00	
02600	DRAINAGE	1.00		0.00	0.00	0.00	0.00	
026201110	PRETX-Surface, 48" x 48"	1.00	Ea.	2,731.25	0.00	0.00	2,731.25	
026201410	Tree, 4" caliper	1.00	Ea.	332.50	220.00	1.00	553.50	
026201510	Tree frame and grate, 6' square	1.00	Ea.	855.00	330.00	2.00	1,187.00	
02900	LANDSCAPING	1.00		0.00	0.00	0.00	0.00	
	Subtotal Sitework			5,027.00	1,230.29	201.25	6,458.54	
	Estimate Total			5,078.21	3,305.92	4,696.25	13,080.38	

BMP-5

Costcode	Description	Quantity	Unit	Material	Labor	Labor Other	
				\$	\$	\$	\$
General]			<u> </u>		
01410	TESTING	1.00		0.00	0.00	0.00	0.00
014101100	Aggregate Infiltration test	2.00	Ea	0.00	270.00	262.50	532.50
015004230	Board-up cover, two sheets plywood	1.00	Ea	51.21	100.63	0.00	151.84
01600	EQUIPMENT RENTAL	1.00		0.00	0.00	0.00	0.00
016001080	Backhoe, diesel, crawler, 1 Cy	3.00	Day	0.00	2,760.00	4,181.25	6,941.25
016001360	Core drill, electric, 2-1/2 HP	1.00	Day	0.00	0.00	88.00	88.00
016001720	Edger, lawn, gas	1.00	Day	0.00	0.00	35.00	35.00
016002660	Saw, concrete, gas	1.00	Day	0.00	0.00	110.00	110.00
016002940	Transit tripod set	1.00	Day	0.00	0.00	53.75	53.75
016003020	Truck, dump, tandem, 12 T load	3.00	Day	0.00	0.00	1,530.00	1,530.00
017001100	Final cleanup	858.00	Sf	0.00	0.00	1,072.50	1,072.50
	Subtotal General			51.21	3,130.63	7,333.00	10,514.84
Sitework							
02050	DEMOLITION	1.00		0.00	0.00	0.00	0.00
020502130	Saw cutting, paving	56.00	Lf	0.00	77.84	25.20	103.04
020502140	Saw cutting, concrete	8.00	Lf	0.00	264.53	5.60	270.13
02060	AGGREGATE AND SOILS	1.00		0.00	0.00	0.00	0.00
020601130	Crushed Stone, Drainage, 1/2"	102.00	Су	2,422.50	0.00	0.00	2,422.50
02070	GEOSYNTHETICS	1.00		0.00	0.00	0.00	0.00
020701110	Geotextiles- Mirafi 160N	880.00	Sf	343.20	0.00	0.00	343.20
02100	SITE PREPARATION	1.00		0.00	0.00	0.00	0.00
021001390	Test Pits	1.00		0.00	0.00	0.00	0.00
02200	EARTHWORK	1.00		0.00	0.00	0.00	0.00
022001010	General excavation	376.00	Су	0.00	3,474.24	2,162.00	5,636.24
022003330	Area backfill, 7' deep	780.00	Sf	0.00	390.00	273.00	663.00
02370	EROSION AND SEDIMENTATION CONTROL	1.00		0.00	0.00	0.00	0.00
023701020	3' Silt fence and haybales	300.00	Lf	825.00	0.00	0.00	825.00
02500	PAVING AND SURFACING	1.00		0.00	0.00	0.00	0.00
025001110	Grade and compact	18.00	Sy	0.00	82.80	46.80	129.60
025002160	Asphalt paving repair	18.00	Sy	290.70	331.20	189.00	810.90
02600	DRAINAGE	1.00		0.00	0.00	0.00	0.00
026001630	Drainage pipe, HDPE, 12" dia	50.00	Lf	855.00	192.50	37.50	1,085.00
026201210	PRETX-Inline, 5' dia, 8' deep	1.00	Ea.	3,325.00	440.00	0.00	3,765.00
026201310	Subsurface chambers 330XL	22.00	Ea.	7,315.00	1,936.00	0.00	9,251.00
02900	LANDSCAPING	1.00		0.00	0.00	0.00	0.00
029001210	Area prep for seeding	87.00	Sy	0.00	32.19	2.61	34.80
029001220	Place top soil, by hand	87.00	Sy	0.00	240.12	0.00	240.12
029002110	Seeding	87.00	Sy	8.70	32.19	1.74	42.63
	Subtotal Sitework			15,385.10	7,493.61	2,743.45	25,622.16
	Estimate Total			15,436.31	10,624.24	10,076.45	36,137.00
	Contingency	25.00	%	3,859.08	2,656.06	2,519.11	9,034.25
	Estimate Total			19,295.39	13,280.30	12,595.56	45,171.25

APPENDIX H: OPERATIONS AND MAINTENANCE PLAN

Operations and Maintenance Plan

Project:

Phase 1: Lincoln Street Subwatershed Nutrient Control Strategies Water Integration for Squamscott-Exeter (WISE) Integrated Plan

Prepared for:

Paul Vlasich, PE Exeter Public Works 13 Newfields Road Exeter, NH 038330

Prepared by:

Robert Roseen, PE, PhD, D.WRE, Jake Sahl, MS Waterstone Engineering, PLLC 2 College Road #1209 Stratham, NH 03885

June 2017



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1.0 INTRODUCTION

The New Hampshire Alteration of Terrain (AoT) regulations (Env-Wq 1500) require the longterm maintenance of stormwater practices, and stipulate the establishment of a mechanism to provide for ongoing inspections and maintenance. This plan has been developed in accordance with Env-Wq 1507.08 Long-Term Maintenance. This Stormwater Management System Operations and Maintenance (O&M) Plan is for Phase 1: Lincoln Street Subwatershed Nutrient Control Strategies, Water Integration for Squamscott-Exeter (WISE) Integrated Plan.

This O&M Plan includes information for three types of BMPs and pretreatment systems: Roadside Right-of-Way (ROW) infiltration, Tree Planters, and Subsurface Infiltration. All systems include pretreatment measures for capture of sediment, trash, and debris. All systems have simple manhole access for cleaning by vactor truck or other means for catch basin cleaning.

Inspections and maintenance are necessary to ensure that the stormwater management systems function as designed. The stormwater management system protects and enhances the stormwater runoff water quality through the removal of sediment and pollutants, and source control significantly reduces the amount of pollutants entering the system.

This O&M Plan identifies responsible parties, reviews the stormwater management systems, provides information on the required maintenance and inspection schedule for each stormwater management method used at the property, discusses debris disposal, and outlines source control procedures. In addition, O&M inspection checklists and site plans are provided in Appendix A: Annual Report Form and O&M Inspection Checklists and Appendix B: Site Plans.

1.1 Responsible Parties

The Owner is responsible for implementing the required reporting, inspection, and maintenance activities identified in this O&M Plan. The Responsible Parties possess the primary responsibility for overseeing and implementing the O&M Plan and assigned Designee who will be responsible for the proper operation and maintenance of the stormwater structures.

1.2 Reporting, Tracking, and Enforcement

The stormwater management system shall be inspected and maintained in accordance with the Operations and Maintenance Plan for the project and the conditions of the NHDES Alteration of Terrain Approval. All record keeping shall be maintained by the identified responsible party and be made available to NHDES or EPA upon request. Inspections should be conducted annually. Reports and inspection forms will be reviewed for completeness with the O&M Plan, inspection findings, and corrective measures, with a report issued by a licensed professional engineer. Maintenance guidance and checklists are provided in Appendix A. Electronic copies will be retained by the Owner for up to 10 years to be made available upon request. All record keeping required by the O&M Plan will be maintained by the Responsible Parties.

These records will include an inspection and maintenance log to document each inspection and maintenance activity and a cataloguing of inspection forms herein. The inspection and maintenance log will include the date on which each inspection or maintenance task was performed, a description of the inspection findings or maintenance completed, and the name of the

inspector or maintenance personnel performing the task. If a maintenance task requires the cleanout of any sediments or debris, the spoils will be disposed of offsite in an appropriate manner. Deficiencies found during inspection will be noted and corrective action undertaken by the owner if needed.

Inspection and Reporting Activity	Timing
<u>1st Year Post Construction</u> Inspect stormwater management and erosion control; examine for 72 hour drawdown.	Every six months and after major storms
<u>2nd Year and Later Post Construction</u> Routine annual inspections per BMP requirements	Annually

Table 1: Schedule for Inspection and Reporting Activities

2.0 STORMWATER MANAGEMENT

This O&M Plan includes information for three types of BMPs and pretreatment systems:

- 1. Roadside Right-of-Way (ROW) infiltration
- 2. Tree Planters
- 3. Subsurface Infiltration

All systems include pretreatment measures for capture of sediment, trash, and debris. All systems have simple manhole access for cleaning by vactor truck or other means for catch basin cleaning. Detailed checklists for inspection and maintenance are provided in Appendix A.

2.2 Tree Planters and Biofilters

The following maintenance items are required for the tree planters, in accordance with Chapter 4-3.4c of the NH Stormwater Manual, Volume 2 (2008). During the six months immediately after construction, the tree planters should be inspected after precipitation events greater than 0.25 inches to ensure that the system is functioning properly. The following activities will be conducted during the first six months after construction and, thereafter, inspections will be conducted on an annual basis:

- Inspections during the first 6 months:
 - Closed pipe system;
 - Curb inlet pretreatment
 - Rip rap apron for inlet and outlet;
 - Filter media
 - Repair/re-vegetate as deficiencies are identified.

- Systems should be inspected annually, and following any rainfall event exceeding 0.5 inches in a 24-hour period during the first year, with maintenance or rehabilitation conducted as warranted by such inspection.
- Pretreatment measures should be inspected annually, and cleaned of accumulated sediment as warranted by inspection.
- Trash and debris should be removed at each inspection
- Vegetation should be inspected annually, and maintained in healthy condition, including pruning, removal and replacement of dead or diseased vegetation, and removal of invasive species.

A checklist for inspection and maintenance is provided in Appendix A.

2.3 Right- of-Way Infiltration Trenches

The following maintenance items are required for the ROW infiltration, in accordance with Chapter 4-3.4c of the NH Stormwater Manual, Volume 2 (2008). During the six months immediately after construction, the tree planters should be inspected after precipitation events greater than 0.25 inches to ensure that the system is functioning properly. The following activities will be conducted during the first six months after construction and, thereafter, inspections will be conducted on an annual basis:

- Inspections during the first 6 months:
 - Closed pipe system;
 - Drop inlet pretreatment basket for trash and debris;
 - Drop inlet piping connection;
 - Infiltration trench monitoring well for drawdown within 72 hrs
- Drop inlet pretreatment basket should be inspected annually, and cleaned of accumulated sediment as warranted by inspection.
- Inspect infiltration trench monitoring well annually after a major storm to ensure it is draining within 72 hours. Corrective action will be taken if drawdown is not evident.
- Inspect for erosion, leakage in liners, and signs of differential settlement.
- Inspect for catch basin pretreatment insert including pipe connections, flexible boot from hanging basket to infiltration trench, and suspension from catch basin frame.

A checklist for inspection and maintenance is provided in Appendix A.

2.4 Subsurface Infiltration

The following maintenance items are required as needed for dry wells at the Site, in accordance with Chapter 4-3.3d of the NH Stormwater Manual, Volume 2 (2008). The following activities will be conducted during the first six months after construction and, thereafter, inspections will be conducted on an annual basis:

• Inspections during the first 6 months:

- Diversion structure;
- Pretreatment chamber;
- Closed pipe system;
- Cultec Chambers Inspection Ports;
- Removal of debris from inlet control structures
- Removal of debris from pretreatment structure
- Inspection of accumulated sediment in Cultec Recharger Inspection Ports
- Removal of accumulated sediment
- Inspection and repair of outlet structures and appurtenances
- Inspection of infiltration components shall occur if a system does not drain within 72hours following a rainfall event. Then a qualified professional should assess the condition of the facility to determine measures required to restore infiltration function, including but not limited to removal of accumulated sediments or reconstruction of the infiltration trench.

A checklist for inspection and maintenance of subsurface infiltration is provided in Appendix A.

3.0 STORMWATER DEBRIS AND SEDIMENT DISPOSAL

Debris and sediment removed during maintenance must be disposed of properly, not left in a location vulnerable to runoff again. Catch basin spoils are not hazardous and should not require contaminated sediment disposal. These materials are commonly used as daily landfill cover if sufficient materials exist. Sediment pollutant concentrations should be below thresholds for categorization as hazardous waste. Vactor liquid could be discharged to a local sanitary sewer or a settling basin.

4.0 **PERSONNEL TRAINING**

All personnel retained for work will be given a copy of this Plan and will receive training in applicable practices for maintenance of the stormwater systems and activities covered in this O&M Plan. The training will include the complete elements of the O&M plan including inspection, corrective measures, and annual reporting.

APPENDIX A: ANNUAL REPORT FORM AND O&M INSPECTION CHECKLISTS

- A.1 ANNUAL REPORTING FORM
- A.2 TREE PLANTER INSPECTION GUIDANCE AND CHECKLIST
- A.3 RIGHT-OF-WAY INFILTRATION GUIDANCE AND CHECKLIST
- A.4 SUBSURFACE INFILTRATION GUIDANCE AND CHECKLIST

ANNUAL REPORT

OPERATIONS AND MAINTENANCE (O&M)

TOWN OF EXETER, NEW HAMPSHIRE STORMWATER MANAGEMENT BMPS

RESPONSIBLE PARTY OR DESIGNEE:

REVIEWING ENGINEER:

ENGINEER SIGNATURE:

DATE:

DATE SUBMITTED TO TOWN:

REPORT SUMMARY

INSPECTION AND REPORTING REQUIREMENTS

This report documents BMP Operations and Maintenance for the Town of Exeter, New Hampshire. All personnel retained for work will be given a copy of this Plan and will receive training for applicable practices for maintenance of the stormwater systems and activities covered in this O&M Plan.

Inspections will be reported annually. Reports and inspection forms will be reviewed for completeness with the O&M Plan, inspection findings, and corrective measures by a professional engineer. An annual report form is provided in Appendix A of the O&M Plan. Electronic copies will be sent to the Town Engineer. Electronic copies will be retained by the Town for such a period as may be required by permits and be made available to appropriate parties upon request. All record keeping required by the O&M Plan will be maintained by the Responsible Parties.

Records will include an inspection and maintenance log to document each inspection and maintenance activity and a cataloguing of inspection forms herein. The inspection and maintenance log will include the date on which each inspection or maintenance task was performed, a description of the inspection findings or maintenance completed, and the name of the inspector or maintenance personnel performing the task. Any deficiencies found during inspection will be noted and corrective action undertaken either by the Town as appropriate.

TOWN CONTACTS FOR SUBMITTAL

Paul Vlasich, Town Engineer:

REQUIRED ANNUAL REPORTING ELEMENTS	INSPECTION COMPLETE	COMMENTS/ CORRECTIVE ACTION
1. Tree Planter Maintenance Checklist		
2. Right-of-Way Infiltration Inspection and Maintenance Checklist		
3. Subsurface Infiltration Inspection and Maintenance Checklist		



COMPLETE

INSPECTION AND MAINTENANCE GUIDANCE FOR TREE PLANTERS

Maintenance of tree planters can typically be performed as part of standard landscaping. Regular inspection and maintenance is critical to the effective operation of tree planters to insure they remain clear of leaves and debris and free draining. This page provides guidance on maintenance activities that are typically required for these systems, along with the suggested frequency for each activity. Individual systems may have more, or less, frequent maintenance needs, depending on a variety of factors including the occurrence of large storm events, overly wet or dry (i.e., drought), regional hydrologic conditions, and the upstream land use.

INSPECTION ACTIVITIES

The most common maintenance activity is the removal of leaves, trash and debris from the pretreatment system. Visual inspections are routine for system maintenance. This includes looking for standing water, accumulated leaves, holes in the soil media, signs of plant distress, and debris and sediment accumulation in the pretreatment system. Tree health is integral to the performance of the system, including infiltration rate and nutrient uptake. Tree care is important to system productivity and health.

ACTIVITY	FREQUENCY
A record should be kept of the time for the system to drain completely after a storm event. The system should drain completely within 72 hours.	
Check to insure the filter surface remains well draining after storm events.	
Remedy : If filter bed is clogged, draining poorly, or standing water covers more than 15% of the surface 48 hours after a precipitation event, then remove top few inches of discolored material. Till or rake remaining material as needed.	
Check pretreatment inlet and outlet for sediment, leaves and debris.	
Remedy : Vactor truck for removal trash and debris from pretreatment device. Access by removal of manhole. Maintenance with the tree planter should rarely be necessary. If needed, rake in and around the system to clear it of debris.	
Check for animal burrows and short circuiting in the system.	After every major storm in the first few
Remedy: Soil erosion from short circuiting or animal boroughs should be repaired when they occur. The holes should be filled and lightly compacted	months, then annually
Check to insure the filter bed does not contain more than 2 inches accumulated material	
Remedy: Remove sediment as necessary. If 2 inches or more of filter bed has been removed, replace media with either mulch or a (50% sand, 20% woodchips, 20% compost, 10% soil) mixture.	
During extended periods without rainfall, inspect tree planter for signs of distress.	
Remedy: tree planter should be watered until established (typical only for first few months) or as needed thereafter.	
Inspect inlets and outlets to ensure good condition and no evidence of deterioration. Check to see if high-flow bypass is functioning.	
Remedy: Repair or replace any damaged structural parts, inlets, outlets, sidewalls.	Annually
Check for robust tree health within the system.	
Remedy: If tree is not established after 1 year, replacement should be considered. Dying branches should be pruned and removed as necessary.	



CHECKLIST FOR INSPECTION OF TREE PLANTERS

Location:	Inspe	ector:	
Date: Time:	Site C	Condition	S:
Date Since Last Rain Event:			
Inspection Items	Satisfactor Unsatisfact	y (S) or tory (U)	Comments/Corrective Action
1. Initial Inspection After Planting			
Tree is stable, roots not exposed	S	U	
Surface is at design level, typically 4" below overflow	S	U	
Overflow bypass / inlet (if available) is functional	S	U	
2. Trash, Debris, and Sediment Removal (1 time a year)			
Litter, leaves, and trash removed from the pretreatment prefilter	S	U	
Sediment accumulation within filter bed less than 2"	S	U	
3. Standing Water (1 time a year & after large storm events during fi	rst year)		
No evidence of standing water after 48 hours	S	U	
4. Short Circuiting & Erosion (1 time a year)			
No evidence of animal burrows or other holes	S	U	
No evidence of erosion	S	U	
5. Drought Conditions (as needed)			
Water tree planter as needed	S	U	
Dead or dying tree	S	U	
6. Overflow Bypass / Inlet Inspection (1 time a year & after large s year)	torm events d	luring first	
No evidence of blockage or accumulated leaves	S	U	
Good condition, no need for repair	S	U	
7. Tree Health (1 time a year)			
Tree health established by first year	S	U	
Robust growth by year 2 or later	S	U	
Prune dying branches	S	U	
Corrective Action Needed			Due Date
1.			
2.			
3.			



INSPECTION AND MAINTENANCE GUIDANCE FOR RIGHT-OF-WAY INFILTRATION

Maintenance of right-of-way infiltration can typically be performed as part of standard landscaping. Regular inspection and maintenance is critical to the effective operation of infiltration systems to insure they remain clear of sediment, trash and debris and are free draining. This page provides guidance on maintenance activities that are typically required for these systems, along with the suggested frequency for each activity. Individual systems may have more, or less, frequent maintenance needs, depending on a variety of factors including the occurrence of large storm events, overly wet or dry (i.e., drought), regional hydrologic conditions, and the upstream land use.

INSPECTION ACTIVITIES

The most common maintenance activity is the removal of leaves, trash and debris from the pretreatment system and visual inspections of the monitoring well within the trench to check for proper drain time.

ACTIVITY	FREQUENCY
A record should be kept of the time for the system to drain completely after a storm event. The system should drain completely within 72 hours.	
Check drop inlet pretreatment within catch basin for sediment and debris. Remedy: Vactor truck for removal trash and debris from pretreatment device. Access by removal of manhole. Maintenance within the infiltration trench component should rarely if ever be necessary.	
Check infiltration trench monitoring well annually after a major storm to ensure it is draining within 72 hours.	
Remedy : Examine inlet to infiltration trench for proper function, monitor the time to drain nearly completely, if the trench fails to drain and remains full, assessment by a qualified engineer is recommended.	After every major storm in the first few months, then annually
Check for erosion, leakage in liners, and signs of differential settlement. Remedy: Monitor issue and address settlement by surface fill. If the issue persists assessment by a qualified engineer is recommended.	
Check catch basin insert pre-filter basket and strainer, pipe connections, flexible boot from hanging basket to infiltration trench, and suspension from catch basin frame. Remedy: Repair or replace parts as necessary.	
Inspect inlets and outlets to ensure good condition and no evidence of	Annually
deterioration. Check to see if high-flow bypass is functioning. Remedy: Repair or replace any damaged structural parts, inlets, outlets, sidewalls.	



CHECKLIST FOR INSPECTION OF RIGHT-OF-WAY INFILTRATION

Location:		Insp	ector:	
Date: Time:		Site	Condition	S:
Date Since Last Rain Event:				
Inspection Items		Satisfactory (S) or Unsatisfactory (U)		Comments/Corrective Action
1. Initial Inspection After Installation				
Pretreatment system is functional including filter basket		S	U	
Primary outlet with flexible boot to infiltration trench is fastene and not leaking	əd	S	U	
Overflow bypass / inlet (if available) is functional		S	U	
2. Drop Inlet Pretreatment (1 time a year)				
Trash, sediment and debris removed from the prefilter system	n	S	U	
3. Infiltration Trench Monitoring Well (1 time a year & after year)				
No standing water after 72 hours		S	U	
4. Erosion, Leakage In Liners, and Signs Of Differential S	Settlemer	nt (1 time a	a year)	
No evidence of leakage from liners or other holes around tren	nch	S	U	
No evidence of differential sediment above infiltration trench				
No evidence of erosion		S	U	
5. Pretreatment Catch Basin Insert Parts (1 time a year)				
Pretreatment pre-filter basket and strainer, pipe connec flexible boot from hanging basket to infiltration trench, suspension from catch basin frame.	ctions, , and	S	U	
6. Overflow Bypass / Inlet Inspection (1 time a year & after year)	large stor	rm events	during first	
No evidence of blockage or accumulated leaves		S	U	
Good condition, no need for repair		S	U	
Corrective Action Needed				Duo Doto
				Due Date
1.				

- 2.
- 3.



INSPECTION AND MAINTENANCE GUIDANCE FOR CULTEC INFILTRATION SYTEMS: RECHARGE CHAMBERS AND SEPARATOR ROW

Regular inspection and maintenance is necessary for the effective operation of infiltration systems. The following guidance is provided for corrective action and maintenance should an infiltration system function inadequately. The Responsible Parties must maintain the infiltration systems in accordance with the minimum design standards. This page provides guidance on maintenance activities that are typically required for infiltration systems, along with a suggested frequency for each activity. Individual infiltration systems may have more, or less, frequent maintenance needs, depending upon a variety of factors including: the occurrence of large storm events; overly wet or dry (i.e., drought) regional hydrologic conditions; and any changes or redevelopment in the upstream land use.

Activity	Frequency
Check to insure the infiltration systems does not clog after storm events	
Check inlets and outlets for debris and high efficiency	
Check to see that the infiltration systems are draining completely within 72 hours after a rain event in Cultec Recharger Inspection Port #1	
Check to see that the infiltration systems are draining completely within 72 hours after a rain event in Cultec Separator Row Port #2	
Check to see that the infiltration bed well does not contain more than 6 inches accumulated material in Cultec Recharger Inspection Port #1	As needed for corrective action
Check to see that the infiltration bed well does not contain more than 6 inches accumulated material in Cultec Separator Row Port #2	
Check to see that the diversion structure is not full of trash, debris, and floatables	
Inspect inlets and outlets to ensure good condition and no evidence of deterioration	
Repair or replace any damaged structural parts, inlets, outlets, valves	



	CHECKLIST FOR INSPECTION OF FOR							
	CULTEC INFILTRATION SYTEMS:							
	RECHARGE CHAMBERS AN	ID SEF	PARATO	R ROW				
Re	egular inspection and maintenance is necessary for the effective	operation	of infiltration	system. The following guidance				
	is provided for corrective action and maintenance should an infiltration system function inadequately.							
Ins	nector:							
Da	te: Time:		Site Condit	ions:				
Da	te Since Last Rain Event:							
Ins	pection Items	Satisfactory (S) or Unsatisfactory (U)		Comments/Corrective Action				
1.	Complete drainage of Cultec Recharger within 72 hours after rain event observed through access port #1	S	U					
2.	Complete drainage of Cultec Separator Row within 72 hours after rain event observed through access port #2	S	U					
3.	Sediment accumulation of Cultec Recharger, 6" or less observed through access port #1	S	U					
4.	Sediment accumulation of Cultec Separator Row, 6" or less observed through access port #2	S	U					
5.	Clogging of Cultec Recharger observed through access port #1	S	U					
6.	Clogging of Cultec Separator Row observed through access port #2	S	U					
7.	Cultec Recharger clear of debris observed through access port #1	S	U					
8.	Cultec Separator Row clear of debris observed through access port #2	S	U					
9.	Diversion structures empty of trash, debris, and floatables observed through manhole	S	U					
10.	Clogging of inlet/outlet structures	S	U					
11.	Cracking, spalling, or deterioration of concrete	S	U					
12.	Animal burrows	S	U					
13.	Undesirable vegetation	S	U					
14.	Undesirable odors	S	U					
15.	Complaints from residents	S	U					
16.	Public hazards noted							
Corrective Action Needed				Due Date				
1.								
2.								
3.								



APPENDIX B: SITE PLANS





MATERIALS LIST		
(SEE COVER SHEET FOR COMBINED PROJECT MATERIALS LIST)		TERIALS LIST)
RECHARGER 330XLSHD STARTER	2	PIECES
RECHARGER 330XLIHD INTERMEDIATE	4	PIECES
RECHARGER 330XLEHD END	2	PIECES
CULTEC NO. 66 WOVEN GEOTEXTILE 7.5' x 300'	10	LINEAL FEET
SEPARATOR ROW MATERIALS LIST		
CULTEC NO. 410 NON-WOVEN GEOTEXTILE 7.5' x 300' (TO WRAP SEPARATOR ROW)	14.22	SQ. YDS
CULTEC NO. 66 WOVEN GEOTEXTILE 7.5' x 300' (BENEATH SEPARATOR ROW)	0.20	ROLLS

CULTE	C REC
	RECH
	RECH
	RECH
	CULT
	CULT

RR CKD CRIPTION S REVIEW S REVIEW DESC 35% 95% DATE 4/9/17 6/4/17 0 - 2 WATERSTONE ENGINEERING INNOVATIVE STORMWATER MANAGEMENT ≤ ÷ Ö WATER INTEGRATION FOR SQUAMSC(ISE) INTEGRATED PLAN (IP) PHASE 1 STREET SUBWATERSHED IT CONTROL STRATEGIES F LINCOLN NUTRIEN DESIGN FOR V EXETER (WI 95% PREPARED FOR: TOWN OF EXETER DEPT. OF PUBLIC WORKS 11 NEWFIELDS ROAD DESIGNED BY: RR DRAFTED BY: CDS CHECKED BY: RR F NEW H ROBERT M. ROSEEN / No. 12215 BIOFILTER BMP-2 DETAILS JOB #: 16928 SCALE: AS SHOWN CONTRCT #: N/A

SUBWATERSHED ROL STRATEGIES

CONTROL

F

RR

CDS

RR

16928

N/A

AS SHOWN

F NEW H ROBERT

HOSEEN

/ NC. 1.221A

TREE-

Ś

LINCOLN NUTRIEN

<u>CUL</u>	<u>TEC RE</u>
	REC
	REC
	REC
	CUL
	CUL

APPENDIX I: 95% BMP DESIGN PACKAGE

95% DESIGN FOR WATER INTEGRATION FOR SQUAMSCOTT - EXETER (WISE) INTEGRATED PLAN (IP) PHASE 1: LINCOLN STREET SUBWATERSHED NUTRIENT CONTROL STRATEGIES

NOTES: UNDERGROUND FACILITIES, STRUCTURES, AND UTILITIES HAVE BEEN PLOTTED FROM AVAILABLE SURVEYS AND RECORDS, AND THEREFORE THEIR LOCATIONS MUST BE CONSIDERED APPROXIMATE ONLY. THERE MAY BE OTHERS, THE EXISTENCE OF WHICH IS PRESENTLY NOT KNOWN. ANYONE USING UTILITY INFORMATION AND DATA PROVIDED HEREIN SHALL CALL DIG SAFE AT 811 SEVENTY TWO (72) HOURS, 3 BUSINESS DAYS IN ADVANCE TO VERIFY THE LOCATION OF UTILITIES PRIOR TO START OF CONSTRUCTION.

PREPARED FOR TOWN OF EXETER, NEW HAMPSHIRE

OWNER: TOWN OF EXETER PAUL VLASICH **TOWN ENGINEER 11 NEWFIELDS ROAD**

GRANT MANAGER: SALLY SOULE NH DEPARTMENT OF ENVIRONMENTAL SERVICES PORTSMOUTH, NH 03881

FUNDED BY: NH DEPARTMENT OF ENVIRONMENTAL SERVICES COASTAL PROGRAM

DIG SAFE: CONTACT DIG SAFE AT 811 HOURS PRIOR TO ANY CONSTRUCTION.

LOCATION MAP

NOT TO SCALE

WATERSTONE ENGINEERING WATER INTEGRATION FOR SQUAMSC ISE) INTEGRATED PLAN (IP) PHASE 1 ATERSHED RATEGIES STRATE SUBWA CONTROL STREET F LINCOLN DESIGN FOR V EXETER (WI 95% PREPARED FOR: TOWN OF EXETER DEPT. OF PUBLIC WORKS 11 NEWFIELDS ROAD DESIGNED BY: RR DRAFTED BY: CDS CHECKED BY: RR NEW / RORFI No. 122 COVER SHEE AND VICINITY MAPS JOB #: 16928 SCALE: AS SHOWN CONTRCT #: N/A

RR RR

LEGEND - EXISTING

(EXISTING - PHASE 1)

SMH (S) DMH 🛈 CB B CBCI TMH 🕕 Ð. -6- \ast \square EMH 🗈 \square \odot 0 \odot Ð *So SG () -0-WMH () WG

SEWER MANHOLE
DRAINAGE MANHOLE
GRATED INLET
CATCH BASIN
CATCH BASIN WITH CURB INLET
TELEPHONE MANHOLE
TELEPHONE POLE
UTILITY POLE
LIGHT POLE
SPOT LIGHT
ELECTRIC MANHOLE
SURVEY MONUMENT
PULL BOX
WHEELCHAIR RAMP (WCR)
BOLLARD
SIGN
VERTICAL BENCHMARK
SHRUB
TREE
CURB STOP
SEWER GATE
FIRE HYDRANT
WATER MANHOLE

WATER GATE

	CONTOUR MAG
	CONTOUR MIN
W	WATER LINE
G	GAS MAIN
TT	UNDERGROUN
— D — D —	STORM DRAIN
	OVERHEAD EL
-0-0-0-0-0-0	FENCE
	TREE LINE
	PROPERTY LII
VSVS	SANITARY VA
S S	SANITARY GR.
FM	SANITARY SE
00000000000000000000000	STONE WALL
	RETAINING WA
<i>GC</i>	GRANITE CUR

VP <u>VP1 OR VP2</u> S <u>SBT OR DBT</u>

CONTOUR MAJOR

CONTOUR MINOR

WATER LINE

GAS MAIN

UNDERGROUND TELEPHONE OR ELECTRIC

STORM DRAINAGE PIPE

OVERHEAD ELECTRIC

FENCE

TREE LINE PROPERTY LINE OR RIGHT-OF-WAY

SANITARY VACUUM SEWER

SANITARY GRAVITY SEWER

SANITARY SEWER FORCE MAIN

RETAINING WALL

GRANITE CURB

VALVE PIT TYPE 1 OR TYPE2

SINGLE OR DUAL BUFFER TANK

LEGEND - EXISTING (EXISTING - SURVEYED AREAS)

· ·	ABUTTERS LINE
	(PER TOWN OF EXETER GIS)
	DIOKADE FENCE
V	PICKET FENCE
<>	CHAIN LINK FENCE
00	OVERHEAD WIRES
ONW	SEWED LINE
S	DRAIN LINE
0	OAS LINE
G	WATER LINE
	WATER LINE
	MAJOR CONTOUR LINE
	MINOR CONTOUR LINE
/ Y Y Y Y Y Y Y Y Y Y Y Y Y	
	SHRUB LINE
	SIGN
0	GRANITE BOUND FOUND
0	IRON PIPE/ROD FOUND
×	POST
	FIRE HYDRANT
WY	WATER CATE VALVE
NSC	WATER SHUTOFF VALVE
GV	GAS GATE VALVE
ŝ	GAS SHUTOFE VALVE
Ũ	CAS METER
GM 🗖	GAS METER
<u>ه</u>	MAIL DUX
	CATCH BASIN (ROUND)
	CATCH BASIN
\bigcirc	DRAIN MANHOLE
\mathbb{M}	MANHULE
E	ELECTRIC MANHOLE
U	IELEPHONE MANHOLE
(W)	WAIER MANHULE

SEWER MANHOLE BOULDER

F 1	TREE STUMP
AT A A A A A A A A A A A A A A A A A A	CONIFEROUS TREE
\odot	DECIDUOUS TREE
A ANA DE	CONIFEROUS SHRUB
⇔	DECIDUOUS BUSH
•	BORING
	PEDESTRIAN MAT
$ \frac{d_{2}^{2}}{d_{2}^{2}} \frac{d_{2}^{2}d_{1}^{2}}{d_{2}^{2}} \frac{d_{1}^{2}}{d_{1}^{2}} \frac{d_{1}^{2}}{d_{1}$	CONCRETE
	LANDSCAPED AREA
	CRUSHED STONE
	BRICK
TYP. EP SWL SYL DYL CONC. VGC SGC CC BB	TYPICAL EDGE OF PAVEMENT SINGLE WHITE LINE SINGLE YELLOW LINE DOUBLE YELLOW LINE CONCRETE VERTICAL GRANITE CURB SLOPED GRANITE CURB CONCRETE CURB BITUMINOUS BERM
IM63/L19	IAX MAP & LOI NUMBER

MATERIAL LEGEND

	INFILTRATION CHAMBER
	BRICK SIDEWALK WITH PATTERN TO MATCH EXISTING
	CONCRETE SIDEWALK
	CONCRETE PAVING
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	GRASS
	STANDARD "HMA" PAVEMENT
÷÷÷÷; 	BIORETENTION SWALE
	TREE PLANTER
	ROW - INFILTRATION GRASSED
	ROW INFILTRATION - TREE TRENCH

DRAWING LIST (CONT)

EROSION AND SEDIMENTATION CONTROL

DRAWING TITLE

COVERSHEET, VICINITY AND LOCATION MAPS

NOTES, ABUTTERS LISTS AND DRAINAGE STRUCTURE TABLES

EROSION AND SEDIMENTATION CONTROL DETAILS AND NOTES

EXISTING CONDITIONS PLAN WITH PROPOSED - PLAN 1 LINCOLN STREET NORTH

EXISTING CONDITIONS PLAN WITH PROPOSED - PLAN 2 LINCOLN STREET SOUTH

EXISTING CONDITIONS PLAN WITH PROPOSED - PLAN 3 WINTER STREET

EXISTING CONDITIONS PLAN WITH PROPOSED - PLAN 4 FRONT STREET

LEGENDS, NOTES AND DRAWING INDEX

ABBREVIATIONS AND LEGENDS

BIOFILTER BMP-1 AND DETAILS

BIOFILTER BMP-2 AND DETAILS

BIOFILTER BMP-5 AND DETAILS

MISCELLANEOUS DETAILS-1

MISCELLANEOUS DETAILS-2

CULTEC DETAILS

RIGHT-OF-WAY INFILTRATION DETAILS

TREE PLANTER AND BIOSWALE DETAILS

DRG No.

GENERAL

16928-G1

16928-G2

16928-G3

16928-G4

16298-ES1

CIVIL

16928-C1

16928-C2

16928-C3

16928-C4

DETAILS

16928-D1

16928-D2

16928-D3

16928-D4

16928-D5

16928-D6

16928-D7

16928-D8

DRA	INAGE	NOT

- PRIOR TO STARTING WORK.

LEGEND	- PROPOSED

(ALL PHASES)

ROADWAY BASELINE
EDGE OF POROUS PAVEMENT
GRANITE CURBING
CAPE COD BERM
LIMIT OF STONE RESERVOIR TRENCH
EDGE TRANSITION DETAIL
REMOVE AND RESET PARKING METER
REMOVE AND RESET PARKING METER
HDPE DRAIN PIPE
HDPE CAP
CATCH BASIN
CATCH BASIN WITH TIP DOWN DETAIL
DRAIN MANHOLE

UTILITY OPERATING AUTHORITIES	
DRAIN/SEWER/WATER	TOWN OF EXETER
TELEPHONE	VERIZON
ELECTRIC	UNITIL

GENERAL NOTES:

- 1. THIS PROJECT HAS BEEN FINANCED BY A DES COASTAL PROGRAM PLANNING GRANT
- BELOW, PERFORMED BY DOUCET LAND SURVEYORS, INC.
- 3. THE CONTRACTOR SHALL BE RESPONSIBLE FOR DETERMINING FINAL LOCATION AND DEPTH OF ALL UTILITIES.
- REPAIR OF ANY EXISTING UTILITIES DAMAGED DUE TO HIS OPERATION.
- WHERE NECESSARY IN ACCORDANCE WITH UTILITY OWNER'S REQUIREMENT WHEN EXCAVATING ADJACENT TO OR CROSSING THAT UTILITY.
- ITEM BASED ON THE QUANTITY OF ACTUAL MATERIAL INSTALLED.
- ENGINEER.
- CONDITIONS AT THE CONTRACTORS EXPENSE.
- REQUIREMENTS AT NO ADDITIONAL COST TO THE OWNER.
- 10. LIMIT OF WORK SHALL BE WITHIN THE PUBLIC RIGHT OF WAY OR AS SHOWN ON THE DRAWINGS.
- 11. PROPOSED CONDITIONS SHOWN HEAVY. EXISTING CONDITIONS SHOWN LIGHT.
- 12. ALL PAVEMENT TO BE SAW-CUT.
- COMMENCES.
- 14. FOR CLARITY PROFILES DO NOT SHOW UTILITIES.
- STREETSCAPE CORRIDOR AS THESE WILL BE IMPORTANT FOR THE SATISFACTORY COMPLETION OF THE PROJECT.
- ELEVATIONS MAY BE AT STEP BASES, WALK SURFACES, AND EXISTING EARTH AND GARDEN AREAS.
- PERCENT ON A CROSS PITCH ACROSS THE STREET PAVEMENT.
- 18. NEW DRAIN INLETS SHALL HAVE THEIR RIM ELEVATIONS SET TO WORK WITH THE REBUILT STREET GRADES.
- FROM SIDE TO SIDE AND SHALL FUNCTION WITH A STREET PAVEMENT THAT HAS THE SAME CHARACTER.

ES:

1. ALL DRAINAGE PIPING SHALL BE 12" INSIDE DIAMETER CORRUGATED HDPE TYPE N-12 PIPE MANUFACTURED BY ADS OR EQUAL SUITABLE FOR H-20 LOADING AT MINIMUM BURIED DEPTH OF 24" UNLESS OTHERWISE NOTED. PIPE SHALL BE SUPPLIED IN 20 FT LENGTHS. JOINTS SHALL BE SOIL TIGHT PUSH ON JOINTS.

2. FINAL LOCATION OF ALL DRAINAGE STRUCTURES TO BE COORDINATED WITH RESIDENT PROJECT REPRESENTATIVE

3. PIPE SHALL BE SLOPED AT A MINIMUM OF 1.0% UNLESS OTHERWISE NOTED.

4. CONTRACTOR IS RESPONSIBLE FOR VERIFYING ALL UTILITIES PRIOR TO EXCAVATION, INCLUDING UTILITIES NOT MARKED BY DIG-SAFE (811), NOT SHOWN ON THE SURVEY, OR NOT MARKED BY THE TOWN. CONTRACTOR IS RESPONSIBLE FOR ANY AND ALL DAMAGES IF AN UNDERGROUND UTILITY IS DAMAGED DURING THE COURSE OF CONSTRUCTION.

5. IN THE EVENT THAT ANY UTILITY, UNDERGROUND OR OVERHEAD, IS DAMAGED DURING CONSTRUCTION, CONTRACTOR SHALL IMMEDIATELY NOTIFY ENGINEER AND THE APPROPRIATE UTILITY COMPANY.

6. ALL CONNECTIONS BETWEEN PRECAST CONCRETE SECTIONS SHALL BE SEALED WITH NON-SHRINK GROUT.

7. CATCH BASINS, INLETS & INFILTRATION BEDS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE STATE DEPARTMENT OF TRANSPORTATION AND ENVIRONMENTAL SERVICES UNLESS OTHERWISE NOTED.

8. ALL PRECAST CONCRETE STRUCTURES SHALL BE RATED FOR AASHTO/H-20 LOADING.

9. ALL MATERIALS USED AND CONSTRUCTION METHODS EMPLOYED ARE TO BE IN ACCORDANCE WITH THE LATEST FEDERAL, STATE AND TOWN REGULATIONS.

10. CONTRACTOR IS RESPONSIBLE FOR DETERMINING DEPTH OF GROUNDWATER AND FOR ALL COSTS ASSOCIATED WITH DEWATERING NECESSARY TO INSTALL STRUCTURES OR PIPING.

11. 13. ANY UNSUITABLE MATERIAL ENCOUNTERED DURING EXCAVATION (ORGANICS, PEAT, ETC.) FOR DRAINAGE STRUCTURES SHALL BE DISPOSED OF BY THE CONTRACTOR AT THEIR EXPENSE. CONTRACTOR IS RESPONSIBLE FOR PROVIDING SUITABLE CLEAN BACKFILL FOR BACKFILL AND COMPACTION.

12. 14. ALL GATE BOXES, PULL BOXES, CATCH BASIN GRATES AND OTHER UTILITY COVERS SHALL BE RAISED AS NEEDED TO BE FLUSH WITH THE TEMPORARY AND FINAL PAVING IF APPLICABLE.

2. THE LOCATIONS OF THE BUILDINGS AND PROPERTY LINES WERE TAKEN FROM TOWN SUPPLIED GIS FILES AND SUPPLEMENTED BY THE FIELD SURVEY, REFERENCED

4. THE CONTRACTOR SHALL CONTACT UTILITY COMPANIES WHEN EXCAVATING IN THE VICINITY OF EXISTING UTILITIES. CONTRACTOR SHALL BE RESPONSIBLE FOR THE

5. THE CONTRACTOR SHALL STRUCTURALLY SUPPORT AND/OR PROTECT WATER MAIN, GAS, STORM SEWER, SANITARY SEWER OR ANY OTHER EXISTING UTILITIES

6. CONTRACTOR SHALL NOTIFY ENGINEER IMMEDIATELY OF ANY INTERFERENCE WITH EXISTING UTILITIES AND THE NEW UTILITIES. IF NEW WORK NEEDS TO BE MOVED OR RELOCATED DUE TO A FIELD CHANGE (EXISTING UTILITIES, TREES, OWNER REQUEST, ETC.) COST FOR RELOCATION SHALL BE INCLUDED IN THE INDIVIDUAL BID

7. CONTRACTOR SHALL BE RESPONSIBLE FOR SUPPORT OF ALL EXCAVATIONS, AS REQUIRED, INCLUDING SHEETING OR BRACING, OR OTHER METHOD APPROVED BY

8. ALL EXISTING ITEMS, INCLUDING BUT NOT LIMITED TO LANDSCAPING, CURBING AND SIDEWALKS DAMAGED BY THE CONTRACTOR SHALL BE RESTORED TO ORIGINAL

9. WHEN THE CONTRACTOR DISTURBS AN AREA WITHIN 5' OF A UTILITY POLE, THE CONTRACTOR SHALL SUPPORT THAT POLE IN ACCORDANCE WITH UTILITY OWNER'S

13. NOT ALL OVERHEAD WIRES AND POWER LINES ARE SHOWN ON THE DRAWINGS. THE CONTRACTOR SHALL FIELD VERIFY LOCATIONS BEFORE CONSTRUCTION

15. PRIOR TO SUBMITTING HIS/HER BID THE CONTRACTOR SHALL VISIT THE SITE TO IDENTIFY AND DOCUMENT WHAT EXISTING CONDITIONS ARE PRESENT ALONG THE

16. NEW SITE GRADES AND ELEVATIONS SHALL BE ESTABLISHED FROM THE ACTUAL EXISTING ELEVATIONS THAT BORDER EACH SECTION OF THE WORK ZONE. THESE

17. THE RECONSTRUCTED STREET PAVEMENT SHALL BE GRADED SO THAT SURFACE DRAINAGE PITCHES TO THE NEW DRAINS. INLETS TO BE SET AT A DESIRED GRADE OF 2 PERCENT, WITH A MINIMUM GRADE OF 1 PERCENT. IN SOME AREAS THE SURFACE GRADE OF THE STREET MAY EXCEED 2 PERCENT BUT SHALL NOT EXCEED 3

19. AT ALL TIMES THE CONTRACTOR SHALL MAINTAIN A SMOOTH CURB LINE THAT FUNCTIONS WITH THE SIDEWALK AND STREET GRADES AND IS WITHOUT SHARP BREAKS, HUMMOCKS, AND HOLLOWS. THE FINAL SURFACE OF THE SIDEWALK SHALL HAVE AN EVEN GRADIENT ALONG THE LINE OF THE STREETSCAPE AS WELL AS

CKD	RR	RR							
DESCRIPTION	35% REVIEW	95% REVIEW							
NO DATE	1 4/9/17	2 6/4/17							
	WATERSTONE			9 GRETA'S WAY	21 KA LHAWI, NH 03883 (p) 603.686.2488				
95% DESIGN FOR WATER INTEGRATION FOR SOURAGOTT -		EXETER (WISE) INTEGRATED PLAN (IP) PHASE 1			NI ITRIENT CONTROL STRATEGIES				
PRE TO DE 11 I DE CHI	PREPARED FOR: TOWN OF EXETER DEPT. OF PUBLIC WORKS 11 NEWFIELDS ROAD DESIGNED BY: RR DRAFTED BY: CDS CHECKED BY: RR								
DF					S, DF				
JOE SC/	3 #: ALE: NTR	СТ #	A	S S	169 HO\)28 VN			

LIST OF ABBREVIATIONS - PROPOSED

AB	ANCHOR BOLT
AC	ASBESTOS CEMENT
ACOUS	ACOUSTICAL (SOUND DEADENING)
ACTL	ACOUSTIC TILE
ADD'L	ADDITIONAL
ADJ	ADJUSTABLE
AFF	ABOVE FINISHED FLOOR
AGGR	AGGREGATE
ALLOW	ALLOWANCE
ALT	ALTERNATE
ALUM	ALUMINUM
APPROX	APPROXIMATE
ARCH	ARCHITECT OR ARCHITECTURAL
AS	AUTOMATED SAMPLER
ASB	ASBESTOS
ASPH	ASPHALT
ASSY	ASSEMBLY
AST	ASPHALT TILE
ATPB	ASPHALT TREATED PERMEABLE BASE
BCV	BUTTERFLY CONTROL VALVE
BF	BLIND FLANGE
BIT	BITUMINOUS
BL or E	BUILDING LINE
BLDG	BUILDING
BLK	BLOCK
BM	BENCH MARK\ BEAM
BO	BOARD
BOF	BOTTOM OF FOOTING
BOT or B	BOTTOM
BP	BASE PLATE
BRG	BEARING
BRK	BRICK
BRZ	BRONZE
BTW	BETWEEN
BU	BUILT UP
CABN CB CC CER CF CFM CI CIP CIRC € CL2 CL or CLR CL2 CL or CLR CLG CLF CL JT CMH CMP CMU CS JT CO COL CONBN CONC CONST CONST CONST CONST CONT CONT CONST CONT CONST CONT CONST CONT CONT CONT CONT CONT CONT CONT CON	CABINET CATCH BASIN CENTER TO CENTER CEMENT CERAMIC CUBIC FEET CUBIC FEET PER MINUTE CAST IRON CAST IRON PIPE CIRCLE, CIRCULAR or CIRCUMFERENCE CENTER LINE CHLORINE CLEAR CEILING CAULKING CONTROL JOINT CLEANOUT CORRUCTION JOINT CLEANOUT COLUMN, COLOR CONBINATION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONSTRUCTION CONTRACTOR CONDUIT COURSE CERAMIC TILE CONTRACT CENTERED COPPER TUBE SIZE COPPER CUBIC INCH CHECK VALVE COLD WATER/ CIRCULAR WASHER CUBIC INCH
DJ	DOUBLE JOINT
DL	DEAD LOAD
DET	DETAIL
DIA, Ø	DIAMETER
DIAG	DIAGONAL
DEFL	DEFLECTION
DIM	DISTRIBUTION, DISTANCE
DIST	DUCTILE IRON
DI	DOZEN
DOZ	DOWN
DN	DOOR
DR	DRAWING
DWG	DOWEL
DWL	DECK HYDRANT
DH	DRAINAGE MANHOLE
DMH	EAST

EA EF EJ EW ECC EFF EL or ELEV ELB ELEC ENAM ENG ENGR ENGR ENT EQUIP EQ or EQUIV EX, EXIST EXC EXH EXP EXT EXTEND OPER EXTR	EACH EACH FACE EXPANSION JOINT EACH WAY ECCENTRIC EFFLUENT ELEVATION ELBOW ELECTRIC ENAMEL ENGINE ENGINE ENGINE ENGINE EQUIPMENT EQUAL or EQUIVALENT EXISTING EXCAVATE EXHAUST EXPANSION EXTERIOR EXTENDED OPERATOR EXTRUDE
FA FC FD FE FF FG FAB FND FIN FIN FIN FIN FIN FIN FIN FIN FIN FLX CON FLG FLR FLCUR FOC FPRF FRP FS FST FT FTG FURR F&C F&G F&G F&G F&G F&G F&G FAB FND FIN FIN FIN FIN FIN FIN FIN FIN FIN FIN	FLANGE ADAPTER FOOT CANDLE/ FLUSHING CONNECTION FLOOR DRAIN/ FIRE DOOR FIRE EXTINGUISHER FAR FACE/ FINISHED FLOOR FIBERGLASS FABRICATE FOUNDATION FINISH FIN RADIATOR FITTING FIXTURE FLASHING/ FLANGE FLEXIBLE CONTAINMENT TUBE FLOORING FLOOR FLUORESCENT FACE OR COLUMN FIREPROOF FIBERGLASS REINFORCED PLASTIC FOOTING STEP FINAL SETTLING TANK FEET FOOTING FURRING/ FURRED FRAME AND COVER FRAME AND GRATING
GC GI GPM GV GWF GA GAL GAL GAL GEN GL GR GR GRAN GRTG GYP BD GYP BD GMU	GENERAL CONTRACTOR GALVANIZED IRON GALLONS PER MINUTE GATE VALVE GLAZED WALL FINISH GAUGE GALLON GALVANIZED GENERATOR GLASS GRADE GRADE GRANITE GRATING GYPSUM BOARD GYPSUM BOARD GLAZED MASONRY UNIT
HVAC HD HDPE HDBD H EXCH HWL HDWR HGT or HT HM HMA H or HORIZ HP H PT HTR HSC HYD	HEATING and VENTILATION HEAVY DUTY HIGH DENSITY POLYETHYLENE HARDBOARD HEAT EXCHANGER HIGH WATER LEVEL HARDWARE HEIGHT HOLLOW METAL HOT MIX ASPHALT HORIZONTAL HORSEPOWER HIGH POINT HEATER HYDRAULIC SYSTEM CENTER HYDRANT
I IF ID INCIN INCL INSUL INT INV IPS ISO I/O JCT JST	IRON INLET INSIDE FACE INSIDE DIAMETER INCINERATOR INCLUDE INSULATION INTERIOR INVERT INTERNAL PIPE SIZE ISOLATION INPUT/ OUTPUT JUNCTION JOIST

JT	JOINT
JAN CLO	JANITOR'S CLOSET
K	1,000 POUNDS (1 KIP)
KC	KEENE'S CEMENT
KGF	KNIFE GATE VALVE
L LF LL LLV/ (H) LWL LAM LAV LT WT LG L PT LT LV	ANGLE LEFT END LINEAR FEET LIVE LOAD LONG LEG VERT./ (HOR.) LOW WATER LEVEL LAMINATE LAVATORY LIGHTWEIGHT LENGTH/ LONG LOW POINT LIGHT LOUVER
M MCC MGD MH MJ MO MAS MATL MAS MATL MAX MECH MEZZ MFR MIN MIR MISC MMH MISC MMH MID MULT	MOTOR MOTOR CONTROL CENTER MILLION GALLONS PER DAY MANHOLE MECHANICAL JOINT MASONRY OPENING MASONRY MATERIAL MAXIMUM MECHANICAL MEMBRANE METAL MEZZANINE MANUFACTURER MINIMUM MIRROR MISCELLANEOUS METHANOL MANHOLE MOUNTING MULTIPLE
N	NORTH
NF	NEAR FACE
NIC	NOT IN CONTRACT
NPT	NATIONAL PIPE THREAD
NTS	NOT TO SCALE
No. or #	NUMBER
NOM	NOMINAL
NAT	NATURAL
NS	NO SMOKING
OF OC OF OF OPNG OPP ORIG OPER	OVERFLOW STRUCTURE ON CENTER OUTSIDE DIAMETER OUTSIDE FACE OPEN TRUSS OPENING OPPOSITE ORIGINAL OPERABLE
P&ID PCF PRV PSF PV PSI POLY, PE PAR PARTN PAT PAVT PC PDC PERF PERP PIV & PLAST PLAS LAM PLBG PLE PLR PLBG PLE PLR PLBG PLE PLR PLS PLB PLB PLB PLE PLR PLS PNL POR PR PR PR PR PR PR PT PVC	PROCESS INSTRUMENTATION DIAGRAM POUNDS PER CUBIC FOOT PRESSURE RELIEF VALVE POUNDS PER SQUARE FOOT PLUG VALVE POUNDS PER SQUARE INCH POLYETHYLENE PARALLEL PARAILEL PARTITION PATTERN PAVEMENT PIECE POWER DISTRIBUTION CENTER PERFORATED PERFORATED PERPENDICULAR PINCH VALVE PLATE/ PROPERTY LINE PLASTER PLACTIS LAMINATE PLUMBING PLANT EFFLUENT PILASTER PLYWOOD PANEL PORCELAIN PAIR PREFABRICATED PROPOSED POINT/ PAINT POLYVINYL CHLORIDE
QT	QUARRY TILE
QTY	QUANTITY
R	RISER, REACTION, RADIUS
RD	ROOF DRAIN\ ROAD
RO	ROUGH OPENING
ROB	RUN OF BANK
RAD	RADIUS/ RADIATOR
RE	RIGHT END

REC RECESS/ RECORD RECIR RECIRCULATION RED REDUCER REF **REFERENCE/ REFRIGERATOR** RCP REINFORCED CONCRETE PIPE REG REGISTER REINF REINFORCING REM REMOVE REP REPAIR REQ'D REQUIRED REV REIVISE RF ROOF RFG ROOFING RL ROOF LEADER RM ROOM RUBB RUBBER RES FLR RESILIENT FLOORING SOUTH SUCTION 'S' SCC SYSTEM CONTROL CENTER SF SQUARE FOOR SJ STEEL JOINT SP STOP PLATE SS STAINLESS STEEL SWD SADL SIDE WATER DEPTH SADDLE SCH SCHEDULE SECT SECTION SEL SELECTION SH SHEET SIM SIMILAR SMP SOI SUMP PUMP SPRAYED ON INSULATION SPEC SPECIFICATION SQ ST SQUARE STREET STAT STATION STL STEEL STL JST STEEL JOIST STOR STORAGE STD STANDARD STIRR STIRRUPS STRUC STRUCTURAL or STRUCTURE SUR SURFACE SUS SUSPENDED/ SUSPENSION SYM SYMMETRICAL SYP SOUTHERN YELLOW PINE SCP STRUCTURAL CLAY PIPE SV SOLENOID VALVE TILE, TREAD or TOP TDH TOTAL DYNAMIC HEAD T/B TOP OF BERM T/D TOP OF DECK T/FTG TOP OF FOOTING T/G TOP OF GROUT T/GRTG TOP OF GRATING T/MAS TOP OF MASONARY T/S TOP OF SLAB T/STL TOP OF STEEL T/W TOP OF WALL THK THICK T&B TOP AND BOTTOM T&G TONGUE AND GROOVE TEL TELEPHONE TEMP TEMPERATURE TR TOILET ROOM TOL TOLERANCE TRANSFORMER TRANS ΤK TANK TYP TYPICAL UNO UNLESS NOTED OTHERWISE UR URINAL ULTRAVIOLET UV VINYL or VERTICAL V VAT VINYL ASBESTOS TILE VT VITRIFIED TILE VERT VERTICAL VS VACUUM SEWER W WATER W/ WITH WAS WAS LINE WI WROUGHT IRON WG WEIR GATE WL WATER LEVEL WO WINDOW OPENING W/O WITHOUT WATER SURFACE WS WELDED WIRE FABRIC WWF WC WATER CLOSET WD WOOD WP WORKING POINT WS WATERSTOP WT WEIGHT W ST WELDED STEEL PIPE WATER VALVE WV WALL HYDRANT WH WP WORKING POINT

STAGING AREA NOTES

- FINAL STAGING AREA LOCATION TO BE DETERMINED WITH THE OWNER PRIOR TO CONSTRUCTION. THE CONTRACTOR IS RESPONSIBLE FOR SECURITY OF ALL MATERIALS AND EQUIPMENT.
- ANY EXISTING PAVEMENT OR OTHER LANDSCAPED AREA DISTURBED DURING CONSTRUCTION SHALL BE RESTORED TO EQUAL OR BETTER CONDITION AT NO ADDITIONAL COST TO THE OWNER.

EROSION & SEDIMENTATION CONTROL NOTES

- 1. CONTRACTOR SHALL COMPLY WITH ALL LOCAL AND STATE REGULATIONS AS APPLICABLE FOR ROAD RECONSTRUCTION.
- 2. ALL EROSION AND SEDIMENTATION CONTROL MEASURES SHALL BE INSPECTED BY THE CONTRACTOR DAILY AND IMMEDIATELY AFTER PERIODS OF RAINFALL. REPAIR AND/OR MAINTENANCE OF SEDIMENTATION AND EROSION CONTROL MEASURES SHALL BE MADE PER THE ENGINEER'S REQUEST AND AS NEEDED. THE CONTRACTOR IS RESPONSIBLE FOR THE IMPLEMENTATION AND MAINTENANCE OF ALL CONTROL MEASURES ON THIS SITE.
- 3. FINAL LOCATION OF ALL SEDIMENTATION CONTROL MEASURES SHALL BE COORDINATED WITH THE TOWN CONSERVATION OFFICE PRIOR TO CONSTRUCTION.
- 4. LAND DISTURBANCE SHALL BE KEPT TO A MINIMUM. RESTABILIZATION WILL BE SCHEDULED IMMEDIATELY AFTER ANY DISTURBANCE.
- 5. SILT FENCES SHALL BE INSTALLED ALONG ANY GRASS ISLAND, WITHIN THE R.O.W., NOT PROTECTED BY CURBING.
- ALL CATCH BASINS IN THE PROJECT AREA SHALL BE PROTECTED WITH FILTER BAG INSERTS THROUGHOUT THE CONSTRUCTION PERIOD AND UNTIL ALL DISTURBED AREAS ARE STABILIZED.
- 7. EROSION AND SEDIMENTATION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO ANY CONSTRUCTION ACTIVITY.
- 8. COVER AND ANCHOR ALL TOPSOIL STOCK PILES WITH STRAW MULCH AND RING WITH SILT FENCE, OR HAY BALE BARRIER.
- 9. DURING CONSTRUCTION, ALL EXPOSED SLOPES THAT WILL NOT RECEIVE PERMANENT SURFACE TREATMENT IMMEDIATELY, AND ALL SOIL STOCKPILES SHALL BE TEMPORARILY SEEDED WITH A MIXTURE OF PERENNIAL RYEGRASS, ANNUAL RYEGRASS AND WINTER GRASS.
- 10. SEDIMENT REMOVAL FROM CONTROL STRUCTURES SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR. SEDIMENT SHALL BE DISPOSED OF IN A MANNER WHICH DOES NOT RESULT IN ADDITIONAL EROSION AND WHICH IS CONSISTENT WITH THE CONTRACT DOCUMENTS AND REGULATORY REQUIREMENTS. ALL SEDIMENT SHALL BE DISPOSED OF AT THE CONTRACTORS EXPENSE.
- 11. THE EROSION AND SEDIMENTATION CONTROL MEASURES DESCRIBED HEREIN ARE INTENDED AS A GENERAL GUIDE FOR THE CONTRACTOR. IT IS THE CONTRACTOR'S RESPONSIBILITY TO PROVIDE ANY AND ALL WORK NECESSARY TO PREVENT EROSION OF SOIL FROM THE CONSTRUCTION SITE. TO PREVENT EROSION, THE CONTRACTOR SHALL PROVIDE SILT FENCES OR OTHER CONTROL MEASURES AS THE NEED ARISES DURING CONSTRUCTION AT NO ADDITIONAL COST TO THE OWNER.
- 12. PAVED ROADWAYS SHALL BE KEPT CLEAN AT ALL TIMES.
- 13. A TEMPORARY CRUSHED STONE PAD OR ROADWAY SHALL BE CONSTRUCTED AT ALL NON-PAVED PARKING AREAS, HEAVY USE AREAS, OR ROADWAYS WHERE THERE IS NO EXISTING PAVEMENT, OR WHERE PAVEMENT HAS BEEN REMOVED.
- 14. CATCH BASINS NOT SHOWN ON SURVEY WITHIN THE CONTRACTOR'S STAGING AREA SHALL BE SUBJECT TO EROSION AND SEDIMENTATION CONTROL MEASURES.

CONSTRUCTION NOTES

- 1. ALL MATERIALS USED AND CONSTRUCTION METHODS EMPLOYED ARE TO BE IN ACCORDANCE WITH THE LATEST FEDERAL, STATE AND TOWN REGULATIONS.
- NOT ALL EXISTING ITEMS (INCLUDING TREES, PLANTERS, HEDGES, SIDEWALKS, FENCE, GUIDE LINES, ETC.) ARE SHOWN ON 2 DRAWINGS. HOWEVER THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY DAMAGE TO EXISTING ITEMS, INCLUDING BUT NOT LIMITED TO LANDSCAPING, CURBING AND SIDEWALKS. ALL DAMAGED ITEMS SHALL BE RESTORED TO THEIR EXISTING CONDITION OR BETTER AND AT NO ADDITIONAL COST TO THE OWNER.
- THE CONTRACTOR SHALL REMOVE AND REPLACE ANY TREES DAMAGED BY HIS CONSTRUCTION OPERATIONS.
- 4. THE CONTRACTOR IS RESPONSIBLE FOR DETERMINING DEPTH OF GROUNDWATER AND FOR ALL COSTS ASSOCIATED WITH DEWATERING NECESSARY TO INSTALL PIPING.
- 5. THE CONTRACTOR SHALL LOCATE, MARK, SAFEGUARD AND PRESERVE ALL SURVEY CONTROL, R.O.W. MONUMENTS, AND INDIVIDUAL PROPERTY CORNER PINS/MONUMENTS IN THE AREA OF CONSTRUCTION. IF DAMAGED, THE CONTRACTOR SHALL REPLACE, AT NO ADDITIONAL COST TO OWNER, INCLUDING SURVEYED CERTIFICATION.
- 6. ALL OPEN TRENCH EXCAVATIONS TO BE PROTECTED BY TRENCH BOX, SHEET PILING OR OTHER METHOD APPROVED BY THE ENGINEER.
- ALL PAVING SHALL BE MAINTAINED BY THE CONTRACTOR, AS-NEEDED THROUGHOUT CONSTRUCTION AND FOR ONE CALENDAR YEAR AFTER CONTRACT COMPLETION. ANY IMPERFECTIONS IN THE PAVEMENT, AS DETERMINED BY THE TOWN OF PROVINCETOWN OR THE ENGINEER. DURING THE GUARANTEE PERIOD SHALL BE RESTORED BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.

SURVEY NOTES

- 1. REFERENCE: LINCOLN STREET AREA EXETER, NH
- 2. FIELD SURVEY PERFORMED BY J.M.L. & L.P.S. OF DOUCET SURVEYING DURING 06/15 USING A TRIMBLE 5603 DR 200 PLUS TOTAL STATION WITH A TDS RANGER DATA COLLECTOR AND A SOKKIA B21 AUTO LEVEL TRAVERSE ADJUSTMENT BASED ON LEAST SQUARE ANALYSIS.
- 3. HORIZONTAL DATUM BASED ON NEW HAMPSHIRE STATE PLANE(2800) NAD83(2011) DERIVED FROM REDUNDANT GPS OBSERVATIONS UTILIZING THE KEYNETGPS VRS NETWORK.
- 4. VERTICAL DATUM IS BASED ON NGVD29 PER DISK B14 1934 ELEV.=37.67'.
- 5. THE ACCURACY OF MEASURED UTILITY INVERTS AND PIPE SIZES/TYPES IS SUBJECT TO NUMEROUS FIELD CONDITIONS, INCLUDING; THE ABILITY TO MAKE VISUAL OBSERVATIONS, DIRECT ACCESS TO THE VARIOUS ELEMENTS, MANHOLE CONFIGURATION, ETC.
- 6. UNDERGROUND UTILITIES MARKED BY TMD SERVICES AND THE TOWN OF EXETER DEPARTMENT OF PUBLIC WORKS.
- 7. EDGE OF SURVEY LIMIT LISTED WHERE LOCATIONS ARE APPROXIMATE AND BASED ON STATE AND TOWN GIS.

CB #1026 RIM ELEV.=47.7' 10" PVC INV.=43.1'

SMH #1028 RIM ELEV.=48.5' (A) 8" CLAY INV.=43.9' (B) NKN, INV = 44.0' (#1084) 8" CLAY INV.=44.0'

CB #1072 RIM ELEV.=48.6' 12" PVC INV.=44.2'

SMH #1084 RIM ELEV.=49.0' (A) 12" CLAY INV.=42.8' (B) 8" CLAY INV.=42.8' (C) 8" ASBESTOS INV.=44.5 (#1028) 8" CLAY INV.=42.7

DMH #1086 RIM ELEV.=49.0' (A) 12" RCP INV.=41.9' (B) 12" RCP INV.=41.8' (C) 12" RCP INV.=41.9

DMH #1091 RIM ELEV.=49.6' (A) 12" RCP INV.=41.7' (#1092) 12" RCP INV.=41.8'

CB #1092 RIM ELEV.=48.6' (#1091) 12" RCP INV.=42.1' (#1099) 12" RCP INV.=41.9'

CB #1099 RIM ELEV.=47.7' (#1026) 10" PVC INV.=41.7' (#1092) 12" RCP INV.=41.7'

CB #1114 RIM FI EV.=48.5' 12" RCP INV.=44.6'

DMH #1142 RIM ELEV.=48.9' (#1033) 12" RCP INV.=44.7 (#1144) 12" PVC INV.=41.7 (#1224) 12" RCP INV.=41.6'

SMH #1143 RIM ELEV.=49.0' (A) 8" CLAY INV.=45.8' (B) 8" CLAY INV.=42.7' (#1145) 10" PVC INV.=42.2 (#1251) 12" CLAY INV.=42.2'

SMH #1145 RIM ELEV.=49.1' (A) 10" PVC INV = 42.4' (#1143) 10" PVC INV.=42.4'

CB #1154 RIM ELEV.=48.6' 6" CIP INV.=44.7

DMH #1144 RIM ELEV.=49.0' (A) 15" RCP INV.=41.5' (#1114) 12" RCP INV.=43.9' (#1142) 12" PVC INV.=41.6 (#1159) 15" RCP INV.=41.6'

DMH #1159 RIM ELEV.=48.8' (#1144) 21" RCP INV.=43.8' (#1163) 21" RCP INV.=44.0

CB #1163 RIM ELEV.=48.3' (A) 21" RCP INV.=44.0' (#1159) 21" RCP INV.=44.0'

CB #1199 RIM ELEV.=46.8' (#1199) 12" CMP INV.=44.2'

CB #1219 RIM ELEV.=46.4' (#1224) 12" RCP INV.=42.7'

DMH #1224 RIM ELEV.=46.7' (A) 8" PVC INV.=41.8' (#1143) 12" RCP INV.=43.2' (#1199) 12" RCP INV.=43.2' (#1219) 12" RCP INV.=41.9'

SMH #1251 RIM ELEV.=46.3' (#1143) 12" CLAY INV.=40.9' (#1317) 12" CLAY INV.=40.9'

SMH #1317 RIM ELEV.=45.8' (UNABLE TO OPEN)

CB #1318 RIM ELEV.=45.3' (#1323) 12" RCP INV.=42.2'

SEWER & DRAINAGE STRUCTURE TABLE

DMH #1323 RIM ELEV.=46.1' (#1401) 12" RCP INV.=41.7' (#1318) 12" RCP INV.=41.8' (#1324) 12" RCP INV.=41.8'

CB #1324 RIM ELEV.=45.7' (#1323) 12" PVC INV.=42.2'

SMH #1400 RIM ELEV.=47.7' (#1317) 12" P\/C IN\/ =38.8' (#1427) UNKN. INV.=37.0' (#1447) UNKN, INV.=36.9'

DMH #1401 RIM ELEV.=47.9' (A) 15" RCP INV.=40.5' (#1323) 12" RCP INV.=40.7' (#1421) 12" RCP INV.=40.9'

MH #1402 RIM ELEV.=48.4' WATER=42.6' SUMP=38.1'

SMH #1416 RIM ELEV.=49.6' (A) 12" PVC INV.=37.6' (B) 10" PVC INV =44.8' (C) UNKN. INV.=38.0' (#1427) 15" PVC INV.=37.5'

SMH #1419 RIM ELEV.=49.5' (UNABLE TO OPEN)

SMH #1420 RIM ELEV.=49.5' NO VISIBLE PIPES SUMP=40.0'

DMH #1421 RIM ELEV.=49.3' (A) 12" RCP INV.=42.1' (#1401) 12" RCP INV.=41.9'

SMH #1427 RIM ELEV.=47.9' (#1400) UNKN. INV.=37.3' (#1416) 15" PVC INV.=37.3'

SMH #1447 RIM ELEV.=47.1' (A) 15" PVC INV.=36.4' (B) 20" RCP INV.=35.9' (#1400) 20" RCP INV.=36.1'

CB #1468 RIM ELEV.=49.7' (A) 12" RCP INV.=43.9' (#1421) 12" RCP INV.=42.7' (#1468) 12" RCP INV.=41.0'

CB #1469 RIM ELEV.=50.7' (#1468) 12" PVC INV.=45.5'

CB #1493 RIM ELEV.=47.9' 15" RCP INV.=44.0' CB #1552

RIM ELEV.=46.5' (A) 15" RCP INV =42 3' (#1493) 15" RCP INV.=42.4' (#1565) 15" RCP INV.=42.2'

DMH #1563 RIM ELEV.=46.2' (A) 24" RCP INV.=34.1' (#1564) UNKN. INV.=34.0' (PIPE BLOCKED) (#1568) 24" RCP INV.=39.3'

CB #1564 RIM ELEV.=45.7' (#1563) 15" RCP INV.=36.9' (#1565) 15" RCP INV.=38.1'

CB #1565 RIM ELEV.=46.4' (#1552) 15" RCP INV.=41.4' (#1564) 15" RCP INV.=41.4'

MH #1566 RIM ELEV.=47.1' (A) 8" CLAY INV.=40.0' (B) 12" UNKN. INV.=40.5'

SMH #1567 RIM ELEV.=47.3' NO VISIBLE PIPES SUMP=41.8'

DMH #1568 RIM ELEV.=47.1' (#1570) 24" RCP INV.=41.0' (#1563) 24" RCP INV.=40.9' (#1626) 12" RCP INV.=41.6'

SMH #1569 RIM ELEV.=47.6' (A) 8" PVC INV.=42.3' (DROP INLET) (B) 8" PVC INV.=39.3' (#1571) 15" PVC INV.=38.5'

DMH #1570 RIM ELEV.=47.2' (A) 24" RCP INV.=42.1' (#1572) 12" PVC INV.=42.8' (#1568) 24" RCP INV.=42.1

SMH #1571 RIM ELEV.=47.7' (A) 12" PVC INV.=39.4' (B) 15" PVC INV.=38.5' (#1569) 15" PVC INV.=38.6

CB #1572 RIM ELEV.=47.2' (#1570) 15" RCP INV.=43.0

CB #1626 RIM ELEV.=50.2' (#1568) 12" RCP INV.=42.1' (#1687) 12" RCP INV.=42.1

SMH #1680 RIM ELEV.=54.7' (A) 6" CLAY INV =45.9' (B) 8" CLAY INV.=44.8' (C) 6" CLAY INV.=44.9'

CB #1687 RIM ELEV.=53.8' (#1823) 12" RCP INV.=45.6' (#1626) 12" RCP INV.=45.4'

SMH #1724 RIM ELEV.=49.9' 6" UNKN. INV.=47.8'

CB #1743 RIM ELEV.=49.9' (#1763) 12" RCP INV.=45.7' (#4427) 12" RCP INV.=45.7'

CB #1763 RIM ELEV.=44.8' (#1743) 12" RCP INV.=42.3' CB #1803

RIM ELEV.=56.6' 12" RCP INV.=51.5' CB #1804 RIM ELEV.=56.3' (A) 12" RCP INV.=50.1 (B) 8" PVC INV.=51.7'

DMH #1805 RIM ELEV.=56.7' (#1803) 12" RCP INV.=49.9' (#1804) 12" RCP INV.=47.6' (#1828) 12" RCP INV.=47.6'

(#1805) 12" RCP INV.=47.6'

DMH #1823 RIM ELEV.=56.1' (#1828) 12" RCP INV.=46.8' (#1687) 12" RCP INV.=46.9

CB #1828 RIM ELEV.=56.3' (#1828) 12" RCP INV.=47.1 (#1823) 12" RCP INV.=47.2'

SMH #1898 RIM ELEV.=57.5' (A) 8" CLAY INV =51 4' (B) FILLED W/SILT

CB #2029 RIM ELEV.=57.3' 12" RCP INV.=53.1

SMH #2062 RIM ELEV.=57.1' (A) 12" UNKN. INV.=48.5' (B) 12" UNKN. INV.=48.5" (C) 8" PVC INV.=48.6'

CB #2252 RIM ELEV.=52.0' 8" HDPE INV.=47.7'

CB #2373 RIM FLEV.=49.5 12" RCP INV.=45.9'

SMH #2418 RIM ELEV.=51.0' (A) 4" UNKN. INV.=47.2' (B) 4" UNKN. INV.=47.2' (#2457) 8" CLAY INV.=46.9'

CB #2454 RIM ELEV.=48.6' (#2573) 12" RCP INV.=44.8' (#2574) 12" PVC INV.=44.8' (#2644) 12" RCP INV.=44.7'

BURIED UNDER PAVEMENT LOCATION PER MARKING CB #2574

SMH #2457

RIM ELEV.=49.0'

12" PVC INV.=44.9' CB #2644 RIM ELEV.=48.3' (#2434) 12" RCP INV.=44.2'

(#4243) 12" RCP INV.=43.9'

CB #4211 RIM ELEV.=47.5' 12" RCP INV.=44.0'

SMH #4241 RIM ELEV.=47.6' (#1742) 8" PVC INV.=42.4' (#2457) 8" PVC INV.=42.4' (#4242) 8" PVC INV.=42.2'

SMH #4242 RIM ELEV.=47.3' (A) 8" PVC INV.=41.0' (#4241) 8" PVC INV.=41.1

CB #4243 RIM ELEV.=46.9' (#2644) 12" RCP INV.=43.5' (#4244) 12" RCP INV.=42.3'

DMH #4244 RIM ELEV.=47.3' (A) 15" RCP INV.=41.8' (#4243) 12" RCP INV.=42.7' (#4427) 12" RCP INV.=42.0'

CB #4427 RIM ELEV.=47.3' (#1743) 12" RCP INV.=44.2' (#4244) 12" RCP INV.=43.0' (#4462) 12" RCP INV.=43.5'

CB #4462 RIM ELEV.=47.4' (#4427) 12" RCP INV.=44.5' MAP 63 LOT 7 NANCY SUTHERLAND IRREV TRUST NANCY SUTHERLAND - TRUSTEE 134 STAGE RD NOTTINGHAM, NH 03290

MAP 63 LOT 8 AMERICAN LEGION CLUB **85 LINCOLN ST** EXETER, NH 03833-0506

MAP 63 LOT 9 TREMONT ST APARTMENTS 30 BIRCH RD DEERFIELD, NH 03037

MAP 63 LOT 252 MCM REALTY TRUST STUART R. PEEKE TRUSTEE PO BOX 1986 EXETER, NH 03833

MAP 73 LOT 1 HAY CREEK EXETER PARTNERS I LLC ATTEN: LEO FICTEAU 90 FRONT ST EXETER, NH 0383

MAP 73 LOT 6 TOWN OF EXETER 10 FRONT STREET EXETER, NH 03833

MAP 73 LOT 7 BARBARA A. PASTER 100 FRONT ST EXETER, NH 03833

MAP 73 LOT 8 TODD M. & CHRISTINE T. PICANSO 102 FRONT ST - APT #2 EXETER, NH 03833

MAP 73 LOT 260 KILIMANJARO LIMITED PARTNERSHIP PO BOX 1986 EXETER, NH 03833

MAP 73 LOT 261 BURTON G. MACARTHUR TRUST MARIE MACARTHUR TRUST **8 LINCOLN ST** EXETER, NH 03833

MAP 73 LOT 262 MARGARET C. GAGE 12 LINCOLN ST EXETER, NH 03833

MAP 73 LOT 263 LORI D. & JEFFREY L. WARRINER 266 FREMONT RD CHESTER, NH 03036

MAP 73 LOT 264 JOHN P. & ANDREA M. RICHARDS 24 LINCOLN ST EXETER, NH 03833

MAP 73 LOT 265 KILIMANJARO LIMITED PARTNERSHIP PO BOX 1986 EXETER, NH 03833

MAP 73 LOT 266 KATHERINE WOOLHOUSE 34 LINCOLN ST EXETER, NH 03833

MAP 73 LOT 268 JAMES E. CONLEY JR 36 LINCOLN ST EXETER, NH 03833

MAP 73 LOT 269 CHRISTOPHER J. CLARKE & SUSAN K. DAVIS 40 LINCOLN STREET EXETER, NH 03833

MAP 73 LOT 270 FREDERICK R. AMEY 42 LINCOLN ST EXETER, NH 03833

MAP 73 LOT 271 ANDREW ROCKWELL 25 GALE DR HAMPTON, NH 03842-1013

MAP 73 LOT 271-1 ANDREW KENT ROCKWELL (65.31%) JANE KENT ROCKWELL REV LIV TRUST (34.69%) 25 GALE ROAD HAMPTON, NH 03842

MAP 73 LOT 272 52 LINCOLN ST LLC 157 COURT ST EXETER, NH 03833

LINCOLN S

BAILLARGEON AR 16 TREMONT ST EXETER, NH 03833 MAP 73 LOT 282 CHRISTINE D. LO

LINCOLN STREET ABUTTERS		CKI
MAP 73 LOT 273 TERRY EUSTIS & MARTIN STOLLAR 157 COURT ST EXETER, NH 03833	MAP 73 LOT 296 MICHAEL J. FARRELL FAMILY TRUST 1992 15 LINCOLN ST EXETER, NH 03833	PTION EVIEW
MAP 73 LOT 274 JAMES BATTLES-TRUSTEE JAMES BATTLES IRREVOCABLE LIVING TRUST 56 LINCOLN ST EXETER, NH 03833	MAP 73 LOT 297 GREGG & VICKI JEAN WILLETT 13 LINCOLN ST EXETER, NH 03833	DESCRI 35% RE 95% RE
MAP 73 LOT 275 TOWN OF EXETER 10 FRONT STREET EXETER, NH 03833	MAP 73 LOT 298 CARY R. EINAUS & JAMES W. MILLS 11 LINCOLN ST EXETER, NH 03833)ATE 1/9/17 5/4/17
MAP 73 LOT 276 ROLAND H. GOUPIL REV. LIVING TRUST LAURIE HUNT GOUPIL REV. LIVING TRUST 37 BELL AVE EXETER NH 03833	MAP 73 LOT 299 SAINT MICHAEL CATHOLIC CHURCH 9 LINCOLN ST EXETER, NH 03833 MAP 73 LOT 300	NO D NO D
MAP 73 LOT 277 BURNHAM AND PFISTER REALTY TRUST 76 LINCOLN ST EXETER, NH 03833	ROMAN CATHOLIC BISHOP OF MANCHESTER 9 LINCOLN ST EXETER, NH 03833 MAP 73 LOT 301	TONE ER MANAGEMENT 3885 8
MAP 73 LOT 278 JOHN S. & ROBI G. JACKSON 1313 LENOX GREENS DR SUN CITY CENTER, FL 33573	GEOFFREY ANDREW VON KUHN 89 FRONT ST EXETER, NH 03833	ATERS GINEE GINEE ETA'S WA' HAM, NH 03 03.686.248
MAP 73 LOT 279 MARY E. PERRY 18 DANIEL ST EXETER, NH 03833		9 GR (p) 6(
MAP 73 LOT 280 EDWARD D. & CATHERINE A. MILLER 14 TREMONT ST EXETER, NH 03833		
MAP 73 LOT 281 BAILLARGEON ARTHUR V 16 TREMONT ST EXETER, NH 03833		- 110
MAP 73 LOT 282 CHRISTINE D. LOWE 18 TREMONT ST EXETER, NH 03833		MSC(SE 1 ED ES
MAP 73 LOT 283 ROBERT T. JOHNSTONE PO BOX 141 EXETER, NH 03833		SQUA PHAS RSH EGI
MAP 73 LOT 284 STEVEN M. & KATHERINE H. SEGAL 21 TREMONT ST EXETER, NH 03833		FOR N (IP) ATEI RAT
MAP 73 LOT 285 ELIJAH P. GOULD 19 TREMONT ST EXETER, NH 03833		D PLA BW/
MAP 73 LOT 286 KERI MARSHALL 47 DEPOT ROAD E.KINGSTON, NH 03827		EGRA RATEI T SU
MAP 73 LOT 287 JOSEPH P. & KIMBERLY C. PHILBRICK MATT & ELIZABETH FOX JACOBS 4 CORTLAND DR GREENLAND, NH 03840		ER INT INTEGI REE
MAP 73 LOT 290 WILLIAM B. & BONNIE L. DEMANCHE 19 DANIEL ST EXETER, NH 03833		R WAT VISE) N ST NT (
MAP 73 LOT 291 JOSEPH R. MIKULSKY & MARY E. CONNOLLY 8 PARKER ST EXETER, NH 03833		N FOR TER (V COLN
MAP 73 LOT 292 SOCIETY OF ST VINCENT DE PAUL - EXETER CHAPT PO BOX 176 EXETER, NH 03833		ESIGI EXET LINC NUT
MAP 73 LOT 293 EXETER SCHOOL DISTRICT 30 LINDEN ST EXETER, NH 03833		95% D
MAP 73 LOT 294 LINCOLN ST CONDO ASSOC. 23 LINCOLN ST EXETER, NH 03833		
MAP 73 LOT 295 PHILIP M. & CHRISTINE S. UTTER 17 LINCOLN ST EXETER, NH 03833		TOWN OF EXETER DEPT. OF PUBLIC WORKS 11 NEWFIELDS ROAD
		DESIGNED BY: RR DRAFTED BY: CDS
		CHECKED BY: RR
		ROBERTT AA. ROSEEN AC. J.221A CENSED CRASED CRASED CRASED
		NOTES, ABUTTERS LIST AND TABLE
		JOB #: 16928 SCALE: AS SHOWN CONTRCT #: N/A

EROSION CONTROL NOTES

GENERAL NOTES:

1. EROSION CONTROL MEASURES SHALL BE INSTALLED AS SHOWN ON THE PLANS.

2. SILT FENCES AND HAY BALE BARRIERS ARE TO BE MAINTAINED AND CLEANED UNTIL ALL SLOPES HAVE BEEN ADEQUATELY STABILIZED.

3. ALL DISTURBED AREAS WHERE TEMPORARY OR FINAL LOAM AND SEED REQUIRED SHALL HAVE A MINIMUM OF 4 INCHES OF LOAM PLACED BEFORE BEING SEEDED AND MULCHED.

4. FILL MATERIAL SHALL BE FREE FROM STUMPS, WOOD, ROOTS, ETC.

5. THE BOTTOM OF ANY SEDIMENT BASINS SHALL BE PERIODICALLY CLEANED, WITH THE SEDIMENT REMOVED TO A SECURE LOCATION SO AS TO PREVENT SILTATION OF NATURAL WATER WAYS AND WETLANDS.

6. AFTER ALL DISTURBED AREAS HAVE BEEN STABILIZED, THE TEMPORARY EROSION CONTROL MEASURES ARE TO BE REMOVED AND ACCUMULATED SEDIMENT DISPOSED IN A SECURE LOCATION.

7. EARTH STOCKPILES ARE TO BE SEEDED AND MULCHED AND HAVE A SILT FENCE INSTALLED ON THE DOWNSLOPE SIDE AS SHOWN ON THE PLANS.

8. EROSION CONTROL MEASURES SHALL BE INSPECTED WEEKLY DURING THE LIFE OF THE PROJECT AND AFTER 0.5" OF RAINFALL. ALL DAMAGED SILT FENCES SHALL BE REPAIRED. SEDIMENT DEPOSITS SHALL PERIODICALLY BE REMOVED AND DISPOSED OF AT AN APPROVED LOCATION.

9. EROSION CONTROL MEASURES SHALL BE REMOVED WHEN THE DISTURBED AREA IS STABILIZED. DISTURBED AREA RESULTING FROM THE SILT FENCE REMOVAL OPERATION SHALL BE PERMANENTLY SEEDED.

10. AN AREA AREA SHALL BE CONSIDERED STABALIZED IF ONE OF THE FOLLOWING HAS OCCURED:

- BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED;
- A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED;
- A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH AS STONE OR RIP RAP HAS BEEN INSTALLED; OR EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.

11. ALL AREAS SHALL BE STABILIZED WITHIN 45 DAYS OF INITIAL DISTURBANCE UNLESS OTHERWISE NOTED.

WINTER NOTES:

1. ALL PROPOSED VEGETATED AREAS WHICH DO NOT EXHIBIT A MINIMUM OF 85% VEGETATIVE GROWTH BY OCTOBER 15TH, OR WHICH ARE DISTURBED AFTER OCTOBER 15TH, SHALL BE STABALIZED BY SEEDING AND INSTALLING EROSION CONTROL BLANKETS ON SLOPES GREATER THAN 3:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT EVENTS.

2. ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85% VEGETATIVE GROWTH BY OCTOBER 15TH, OR WHICH ARE DISTURBED AFTER OCTOBER 15TH, SHALL BE STABALIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS.

3. AFTER NOVEMBER 15TH, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3 INCHES OF CRUSHED GRAVEL PER NHDOT ITEM 304.3.

STANDARD STABILIZATION NOTE: FOLLOWING INITIAL SOIL DISTURBANCE OR REDISTURBANCE, PERMANENT OR TEMPORARY STABILIZATION SHALL BE COMPLETED WITHIN SEVEN (7) CALENDAR DAYS AS TO THE SURFACE OF ALL PERIMETER CONTROLS, DIKES, SWALES, DITCHES, PERIMETER SLOPES, AND ALL SLOPES GREATER THAN 3 HORIZONTAL TO 1 VERTICAL (3:1), AND FOURTEEN (14) DAYS AS TO ALL OTHER DISTURBED OR GRADED AREAS ON THE PROJECT SITE.

1. CONTRACTOR/DEVELOPER SHALL NOTIFY NEW HAMPSHIRE DEPARTMENT OF ENVIRONMENTAL SERVICES (NHDES) AND TOWN OF RINDGE 2 WEEKS PRIOR TO START OF CONSTRUCTION.

2. SCHEDULE PRE CONSTRUCTION MEETING. REVIEW AND BECOME FAMILIAR WITH ALL PERMITS.

3. A SOURCE OF OFFSITE FILL MATERIAL SHALL BE IDENTIFIED AND APPROVED BY THE OWNER/INSPECTOR/ENGINEER.

4. INSTALL STABILIZED CONSTRUCTION ENTRANCE (1 DAY).

DAYS).

DAYS).

8. CUT AND CLEAR TREES.

9. CLEAR AND DISPOSE OF DEBRIS.

12. BEGIN PERMANENT AND TEMPORARY SEEDING AND MULCHING. ALL CUT AND FILL SLOPES SHALL BE SEEDED AND MULCHED WITHIN 72 HOURS OF THEIR CONSTRUCTION.

13. DAILY, OR AS REQUIRED, CONSTRUCTED TEMPORARY BERMS, DRAINS, DITCHES, SILT FENCES, SEDIMENT TRAPS, ETC., MULCH AND SEED AS REQUIRED.

PRECISE OR NECESSARILY ACCURATE. NO WORK WHATSOEVER SHALL BE UNDERTAKEN ON THIS SITE USING THIS PLAN TO LOCATE THE ABOVE SERVICES. CONSULT WITH THE PROPER AUTHORITIES CONCERNED WITH THE SUBJECT SERVICE LOCATIONS FOR INFORMATION REGARDING SUCH, CALL DIG-SAFE AT 81

5. INSTALL STANDARD INLET PROTECTION DEVICES ON EXISTING STORM DRAIN AND CATCH BASIN INLETS (2

6. CLEAR AND ROUGH GRADE (ONLY WHERE NECESSARY) FOR THE INSTALLATION OF PERIMETER SILT FENCE (3

7. INSTALL REMAINDER OF SILT FENCE ON EXISTING WWTP AND EFFLUENT DISPOSAL SITE (1 DAY).

10. GRADE AND GRAVEL ROADWAYS AND PARKING AREAS -ALL ROADS AND PARKING AREAS SHALL BE STABILIZED IMMEDIATELY AFTER GRADING.

11. CONTRACTOR TO CONSTRUCT ONLY ONE SAND BED AT A TIME TO MINIMIZE SITE DISTURBANCE.

- CATCH BASIN

GRATE

SEDIMENTATION CONTROL AT CATCH BASIN

NOT TO SCALE

NOTES:

1. EROSION CONTROL MATS MANUFACTURED BY NORTH AMERICAN GREEN'S, MODEL S150 & SC150 AND INSTALLED PER MANUFACTURERS RECOMMENDATIONS.

2. USE S150 EROSION CONTROL MATS ON 3:1 TO 2:1 SLOPES. USE SC150 EROSION CONTROL MATS ON 2:1 TO 1:1 SLOPES.

MIN. DEPTH) 12" MIN. (TYP) WIRE MESH

- COARSE AGGREGATE (12"

GRAVEL AND WIRE MESH DROP INLET SEDIMENT FILTER NOT TO SCALE

1. A WIRE MESH SHOULD BE PLACED OVER THE DROP INLET OR CURB OPENING SO THAT THE ENTIRE OPENING AND A MINIMUM OF 12" OF THE OPENING ARE COVERED BY THE MESH. THE MESH MAY BE ORDINARY HARDWARE CLOTH OR WIRE MESH WITH OPENINGS UP TO 1/2".

2. THE WIRE MESH SHOULD BE COVERED WITH CLEAN COARSE AGGREGATE SUCH AS SEWER

3. THE COARSE AGGREGATE SHOULD EXTEND AT LEAST 18" ON ALL SIDES OF THE DRAIN

2. WIDTH - 10' MINIMUM, SHOULD BE FLARED AT THE EXISTING ROAD TO PROVIDE A TURNING RADIUS.

3. GEOTEXTILE FABRIC (MIRAFI 180N OR EQUAL) SHALL BE PLACED OVER THE EXISTING GROUND PRIOR TO

4. STONE - CRUSHED AGGREGATE (2" TO 3") OR RECLAIMED OR RECYCLED CONCRETE EQUIVALENT SHALL BE PLACED AT LEAST 6" DEEP OVER THE LENGTH AND WIDTH OF THE ENTRANCE.

5. SURFACE WATER - ALL SURFACE WATER FLOWING TO OR DIVERTED TOWARD CONSTRUCTION ENTRANCES SHALL BE PIPED THROUGH THE ENTRANCE, MAINTAINING POSITIVE DRAINAGE. PIPE INSTALLED THROUGH THE STABILIZED CONSTRUCTION ENTRANCE SHALL BE PROTECTED WITH A MOUNTABLE BERM WITH 5:1 SLOPES AND A MINIMUM OF 6" OF STONE OVER THE PIPE. PIPE HAS TO BE SIZED ACCORDING TO THE DRAINAGE. WHEN THE SCE IS LOCATED AT A HIGH SPOT AND HAS NO DRAINAGE TO CONVEY A PIPE WILL NOT BE NECESSARY. PIPE SHOULD BE SIZED ACCORDING TO THE AMOUNT OF RUNOFF TO BE CONVEYED. A 6" MINIMUM WILL BE REQUIRED.

6. LOCATION - A STABILIZED CONSTRUCTION ENTRANCE SHALL BE LOCATED AT EVERY POINT WHERE CONSTRUCTION TRAFFIC ENTERS OR LEAVES A CONSTRUCTION SITE. VEHICLES LEAVING THE SITE MUST TRAVEL OVER THE ENTIRE LENGTH OF THE STABILIZED CONSTRUCTION ENTRANCE.

STABILIZED CONSTRUCTION ENTRANCE

NOT TO SCALE

CKD	RR	RR							
DESCRIPTION	35% REVIEW	95% REVIEW							
NO DATE	1 4/9/17	2 6/4/17							
	WATERSTONE	ENGINEERING INNOVATIVE STORMWATER MANAGEMENT	Q CRETA'S M/AV	STRATHAM NH 03885	(p) 603.686.2488				
95% DESIGN FOR WATER INTEGRATION FOR SOLIAMSCOTT -		EXELER (WISE) IN LEGRALED PLAN (IP) PHASE 1	I INCOLN STRFFT SURWATERSHED		NI ITRIENT CONTROL STRATEGIES				
PRE TO' DE 11 DES DR/	EPA WN PT. (NEW SIGI AFT	RED OF E OF P /FIEL NED ED B	FOR XETE UBLIC .DS R BY: Y:	: ER C W ROA					
	DRAFTED BY: CDS CHECKED BY: RR CHECKED BY: RR NO. 12215 CHECKED BY: RR ROBERT M. ROBERT M. ROBER								
JOE SC/	3 #: ALE:		AS	SF	169 101	928 VN			
COI	NTR	CT #			N	J/A			

LOCATE THE ABOVE SERVICES. CONSULT WITH THE PROPER AUTHORITIES CONCERNED WITH THE SUBJECT SERVICE LOCATIONS FOR INFORMATION REGARDING SUCH. CALL DIG-SAFE AT 811.

:3)	Soil Type	Drainage Area (acres)	Annual TN Load (lbs)	System Size
	А	0.20	2.5	1/2" WQV
	А	0.13	1.7	1/2" WQV
	А	0.27	3.4	1/2" WQV
	А	0.22	2.9	1/2" WQV
	А	0.24	2.4	1/2" WQV
	А	0.78	7.2	1/2" WQV
	А	1.20	9.1	1/2" WQV
	А	0.70	5.6	1/2" WQV
	А	0.20	1.3	1/2" WQV

/ity	Depth to Test Pit ID Bedrock		Field Technician	Site Visit Date
	32+ inches	TP4 / 5	A. Moskal, M. Roseen	12/6/2016
	32+ inches	TP4	A. Moskal, M. Roseen	12/6/2016

10 Storer Street (Riverview Suite) Kennebunk, ME (207) 502-7005 http://www.doucetsurvey.com

for Construction unless Signed and Sealed For Construction.

t Invert Elevation (ft)	Length (ft)	Width (ft)	Depth (ft)	Surface Area (ft2)	Storage Volume (ft3) Soil Type Drainage Area (acres) Annual TN Load		Annual TN Load (lbs)	System Size	
	0.7	. ,		. ,			c		
44.6	55	5	4	275	440	А	1.60	13.9	1/2" WQV
45.3	4	5	4	20	32	А	0.24	1.4	1/2" WQV

Soil Type	Hydrologic Soil Group	Hydraulic Conductivity (SSSNNE)	Depth to Bedrock	Test Pit ID	Field Technician	Site Visit Date
Fine Sandy Loam	А	0.6 - 6.0 in/hr	32+ inches	TP4	A. Moskal, M. Roseen	12/6/2016
Fine Sandy Loam	А	0.6 - 6.0 in/hr	32+ inches	TP4	A. Moskal, M. Roseen	12/6/2016

BMP #	ВМР Туре	Inlet Invert Elevation (ft)	Length (ft)	Width (ft)	Depth (ft)	Surface Area (ft2)	Storage Volume (ft3)	Soil Type	Drainage Area (acres
1	Subsurface Infiltration	56.9	40	35	8	1400	4,816	А	12.88
2*	Subsurface Infiltration	49.2	50	24	10	1200	5,696	A	24.56

BMP ID	Soil Type	Hydrologic Soil Group	Hydraulic Conductivity (SSSNNE)	Depth to Bedrock	Test Pit ID	Field Technician	Site Visit Date
BMP 1	Charlton Fine Sandy Loam	А	0.6 - 6.0 in/hr	54+ inches	TP1	A. Moskal, M. Roseen	11/28/2016
BMP 2	Charlton Fine Sandy Loam	А	0.6 - 6.0 in/hr	41+ inches	TP2	A. Moskal, M. Roseen	12/6/2016

LEGEND - EXISTING (EXISTING - SURVEYED AREAS)

FRONTSTREET

	ABUTTERS LINE
	(PER TOWN OF EXETER GIS)
ooo	STOCKADE FENCE
v	PICKET FENCE
	- POST & RAIL FENCE
0 0	- CHAIN LINK FENCE
OHW	- OVERHEAD WIRES
S	- SEWER LINE
D	
C	
W	WATED LINE
100	MATER LINE
	MAJOR CONTOUR LINE
	MINOR CONTOUR LINE
./ ¥ ¥ ¥ ¥ ¥ ¥ ¥ ¥ ¥	· IREE LINE
	SHRUB LINE
C.	UTILITY POLE
	UTILITY POLE & GUY WIRE
	SIGN CRANITE ROUND FOUND
	IPON DIDE /DOD FOUND
	POST
	FIRE HYDRANT
Ŵ	
×	WATER GATE VALVE
No.	WATER SHUTOFF VALVE
×	GAS GATE VALVE
Õ	GAS SHUTOFF VALVE
см П	GAS METER
	MAIL BOX
æ	CATCH BASIN (ROUND)
	CATCH BASIN
	MANHOLE
	TELECTING MANHOLE
	ILLEFITUNE MANHOLE
· · ·	WATER MANHOLE
S	SEWER MANHOLE
W	ROOFDEK

TREE STUMP CONIFEROUS TREE DECIDUOUS TREE CONIFEROUS SHRUB DECIDUOUS BUSH BORING PRETX

PEDESTRIAN MAT CONCRETE

LANDSCAPED AREA CRUSHED STONE

BRICK

TYP.TYPICALEPEDGE OF PAVEMENTSWLSINGLE WHITE LINESYLSINGLE YELLOW LINEDYLDOUBLE YELLOW LINECONC.CONCRETEVGCVERTICAL GRANITE CURBSGCSLOPED GRANITE CURBCCCONCRETE CURBBBBITUMINOUS BERMTM63/L19TAX MAP & LOT NUMBER

NOTE: ALL ELECTRIC, GAS, TEL. WATER, SEWER AND DRAIN SERVICES ARE SHOWN IN SCHEMATIC FASHION, THEIR LOCATIONS ARE NOT PRECISE OR NECESSARILY ACCURATE. NO WORK WHATSOEVER SHALL BE UNDERTAKEN ON THIS SITE USING THIS PLAN TO LOCATE THE ABOVE SERVICES. CONSULT WITH THE PROPER AUTHORITIES CONCERNED WITH THE SUBJECT SERVICE LOCATIONS FOR INFORMATION REGARDING SUCH. CALL DIG-SAFE AT 811.

LEGEND - EXISTING (EXISTING - SURVEYED AREAS)

□ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □	ABUTTERS LINE (PER TOWN OF EXETER GIS) STOCKADE FENCE PICKET FENCE POST & RAIL FENCE CHAIN LINK FENCE OVERHEAD WIRES SEWER LINE DRAIN LINE GAS LINE WATER LINE WATER LINE WATER LINE MAJOR CONTOUR LINE NINOR CONTOUR LINE SHRUB LINE UTILITY POLE & GUY WIRE SIGN GRANITE BOUND FOUND IRON PIPE/ROD FOUND IRON PIPE/ROD FOUND POST FIRE HYDRANT WATER GATE VALVE WATER SHUTOFF VALVE GAS METER MAIL BOX CATCH BASIN (ROUND) CATCH BASIN DRAIN MANHOLE MANHOLE ELECTRIC MANHOLE	 ✓ ✓
	ELECTRIC MANHOLE TELEPHONE MANHOLE WATER MANHOLE SEWER MANHOLE BOULDER	

TREE STUMF	
CONIFEROUS	TREE
DECIDUOUS	TREE
CONIFEROUS	SHRUB
DECIDUOUS BORING	BUSH
PEDESTRIAN	MAT
CONCRETE	
LANDSCAPE) AREA
CRUSHED ST	TONE
BRICK	
TYPICAL EDGE OF PA SINGLE WHIT SINGLE YELL DOUBLE YELL CONCRETE VERTICAL GF SLOPED GRA CONCRETE C BITUMINOUS TAX MAP &	VEMENT TE LINE LOW LINE LOW LINE RANITE CURB ANITE CURB CURB BERM LOT NUMBER

TEST PITS

TEST PITS MUST BE CONDUCTED AT EACH LOCATION TO VERIFY SOILS AND SEASONAL HIGH WATER TABLE

MATERIAL LEGEND

INFILTRATION CHAMBER BRICK SIDEWALK WITH PATTERN TO MATCH EXISTING CONCRETE SIDEWALK CONCRETE PAVING GRASS

STANDARD "HMA" PAVEMENT

BIORETENTION SWALE TREE PLANTER

ROW - INFILTRATION GRASSED

ROW INFILTRATION - TREE TRENCH

PRETX STRUCTURE -----

INSTALL CONSTRUCTED

NOTES: 1. ALL ELECTRIC, GAS, TEL. WATER, SEWER AND DRAIN SERVICES ARE SHOWN IN SCHEMATIC FASHION, THEIR LOCATIONS ARE NOT PRECISE OR NECESSARILY ACCURATE. NO WORK WHATSOEVER SHALL BE UNDERTAKEN ON THIS SITE USING THIS PLAN TO LOCATE THE ABOVE SERVICES. CONSULT WITH THE PROPER AUTHORITIES CONCERNED WITH THE SUBJECT SERVICE LOCATIONS FOR INFORMATION REGARDING SUCH. CALL DIG-SAFE AT 1-888-DIG-SAFE.

BASE MAP INFORMATION TAKEN FROM PLAN ENTITLED FRONT STREET CROSS WALK CONCEPT DRAWING L-1 DATED JANUARY 21, 2014 AS PREPARED BY KZLA KYLE ZICK LANDSCAPE ARCHITECTURE, INC. 36 BROWNFIELD STREET, BOSTON, MA 02108.

BMP #	ВМР Туре	Inlet Invert Elevation (ft)	Length (ft)	Width (ft)	Depth (ft)	Surface Area (ft2)) Storage Volume (ft3)	Soil Type	Drainage Area (acres)	Annual TN Load (lbs)	System Size
5	Subsurface Infiltration	36.7	78	10	10	780	3,822	А	20.29	138.3	1/4" WQV
		BMP ID	Soil 1	Soil Type H		rologic Soil H Group	lydraulic Conductivity (SSSNNE)	Depth Bedroo	to Test Pit ID ck	Field Technician	Site Visit Date
				Constructions							42/7/2046

Inlet Invert Elevation	n (ft) Length (ft)	Width (ft)	Depth (ft)	Surface Area (ft2)	Storage Volume (ft3)	Soil Type	Dra	ainage Area (acres)	Annual TN Load (lbs)	System Size
36.7	78	10	10	780	3,822	А		20.29	138.3	1/4" WQV
BMP ID	Soil	Гуре	Hydı	ologic Soil H	ydraulic Conductivity (SSSNNF)	Conductivity Depth to		Test Pit ID	Field Technician	Site Visit Date
					(5551112)		CK			
BMP 5	Charlton Fine	Sandy Loa	m	A	0.6 - 6.0 in/hr	28+ inc	hes	TP6	A. Moskal, M. Roseen	12/7/2016

EXISTING AND PROPOSED CONDITIONS PLAN - 4 FRONT STREET SCALE: 1" = 40'

MATERIALS LIST						
(SEE COVER SHEET FOR COMBINED PR	OJECT MA	TERIALS LIST)				
RECHARGER 330XLSHD STARTER	2	PIECES				
RECHARGER 330XLIHD INTERMEDIATE	4	PIECES				
RECHARGER 330XLEHD END	2	PIECES				
CULTEC NO. 66 WOVEN GEOTEXTILE 7.5' x 300'	10	LINEAL FEET				
SEPARATOR ROW MATER	RIALS LIST					
CULTEC NO. 410 NON-WOVEN GEOTEXTILE 7.5' x 300' (TO WRAP SEPARATOR ROW)	14.22	SQ. YDS				
CULTEC NO. 66 WOVEN GEOTEXTILE 7.5' x 300' (BENEATH SEPARATOR ROW)	0.20	ROLLS				

CULTE	EC REC
	RECH
	RECH
	RECH
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	CULT

CKD RR RR CRIPTION S REVIEW S REVIEW DESC 35% 95% DATE 4/9/17 6/4/17 0 - 2 WATERSTONE ENGINEERING INNOVATIVE STORMWATER MANAGEMENT ≤ ÷ Ö WATER INTEGRATION FOR SQUAMSC(ISE) INTEGRATED PLAN (IP) PHASE 1 STREET SUBWATERSHED IT CONTROL STRATEGIES F LINCOLN NUTRIEN DESIGN FOR V EXETER (WI 95% PREPARED FOR: TOWN OF EXETER DEPT. OF PUBLIC WORKS 11 NEWFIELDS ROAD DESIGNED BY: RR DRAFTED BY: CDS CHECKED BY: RR F NEW H ROBERT M. ROSEEN / No. 12215 BIOFILTER BMP-2 DETAILS JOB #: 16928 SCALE: AS SHOWN CONTRCT #: N/A




SUBWATERSHED ROL STRATEGIES

CONTROL

F

RR

CDS

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16928

N/A

AS SHOWN

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LINCOLN NUTRIEN







- 1	
	TEST PITS
	TEST PITS MUST BE
	CONDUCTED AT EACH LOCATION
	TO VERIFY SOILS AND
	SEASONAL HIGH WATER TABLE

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	CUL

MATERIALS LIST			
(SEE COVER SHEET FOR COMBINED PROJECT MATERIALS LIST)			
RECHARGER 330XLSHD STARTER	2	PIECES	
RECHARGER 330XLIHD INTERMEDIATE	4	PIECES	
RECHARGER 330XLEHD END	2	PIECES	
CULTEC NO. 66 WOVEN GEOTEXTILE 7.5' x 300'	10	LINEAL FEET	
SEPARATOR ROW MATERIALS LIST			
CULTEC NO. 410 NON-WOVEN GEOTEXTILE 7.5' x 300' (TO WRAP SEPARATOR ROW)	14.22	SQ. YDS	
CULTEC NO. 66 WOVEN GEOTEXTILE 7.5' x 300' (BENEATH SEPARATOR ROW)	0.20	ROLLS	





CONSTRUCTION NOTES:

EXAMINATION

- A. VERIFY LAYOUT AND ORIENTATION OF BIORETENTION AREA AND CONNECTIONS B. VERIFY EXCAVATION BASE IS READY TO RECEIVE WORK AND EXCAVATIONS. DIMENSIONS. AND
- ELEVATIONS ARE AS INDICATED ON DRAWINGS.

2. PREPARATION

- A. CALL DIGSAFE AT 811 NOT LESS THAN THREE WORKING DAYS BEFORE PERFORMING WORK. REQUEST UNDERGROUND UTILITIES TO BE LOCATED AND MARKED WITHIN AND SURROUNDING CONSTRUCTION AREAS.
- C. IDENTIFY REQUIRED LINES, LEVELS, CONTOURS, AND DATUM.
- D. CLEAR AND GRUB THE PROPOSED BIORETENTION AREA.
- 3. EXCAVATION
 - A. EXCAVATE BIORETENTION AREA IN ACCORDANCE WITH GENERAL NOTES AND SPECIFICATIONS. B. TO MINIMIZE COMPACTION, WORK EXCAVATORS OR BACKHOES FROM THE SIDES TO EXCAVATE THE BIORETENTION AREA TO ITS APPROPRIATE DESIGN DEPTH AND DIMENSIONS. USE EXCAVATING EQUIPMENT WITH ADEQUATE REACH SO THEY DO NOT WORK IN THE FOOTPRINT OF THE BIORETENTION AREA. IF APPLICABLE AND PER THE ENGINEERS DIRECTION USE A CELL CONSTRUCTION APPROACH IN LARGER BIORETENTION BASINS, WHEREBY THE BASIN IS SPLIT INTO 500 TO 1000 SQUARE FOOT TEMPORARY CELLS WITH A 10 TO 15 FOOT EARTH BRIDGE IN BETWEEN, SO THAT CELLS CAN BE EXCAVATED FROM THE SIDE.
 - C. EXCAVATE AND SEAL ANY PRETREATMENT CELLS AND/OR SEDIMENT FOREBAYS FIRST AND SEALED TO TRAP SEDIMENTS PER THE DRAWINGS.
 - ROUGH GRADE THE BIORETENTION AREA DURING GENERAL CONSTRUCTION. EXCAVATE THE BIORETENTION FACILITIES TO WITHIN 1 FOOT OF UNDERDRAIN BOTTOM.
 - E. IF THE BIORETENTION AREA IS TO BE USED AS A TEMPORARY DRAINAGE STORAGE BASIN DURING THE EARLY STAGES OF PROJECT CONSTRUCTION, THE SIDE SLOPES SHOULD BE TEMPORARILY STABILIZED AND SILT FENCE INSTALLED ALONG THE TOE OF THE ROUGH GRADED BIORETENTION SLOPES TO MINIMIZE EXCESSIVE SEDIMENTATION OF THE BIORETENTION FLOOR.
- COMPACTION
 - A. MINIMIZE COMPACTION OF BOTH THE BASE OF THE BIORETENTION AREA AND THE REQUIRED BACKFILL. COMPACTION WILL SIGNIFICANTLY CONTRIBUTE TO DESIGN FAILURE.
 - B. USE EXCAVATOR OR BACKHOES TO EXCAVATE THE BIORETENTION AREA C. IF THE BIORETENTION AREA IS EXCAVATED USING A LOADER, USE ONLY WIDE TRACK OR MARSH TRACK EQUIPMENT, OR LIGHT EQUIPMENT WITH TURF TYPE TIRES. USE OF EQUIPMENT WITH NARROW TRACKS OR NARROW TIRES, RUBBER TIRES WITH LARGE LUGS, OR HIGH PRESSURE TIRES CAUSE EXCESSIVE COMPACTION RESULTING IN REDUCED INFILTRATION RATES AND STORAGE VOLUMES AND IS NOT ACCEPTABLE.
 - D. COMPACTION CAN BE ALLEVIATED AT THE BASE OF THE BIORETENTION FACILITY BY USING A PRIMARY TILLING OPERATION SUCH AS A CHISEL PLOW, RIPPER, OR SUBSOILER. THESE TILLING OPERATIONS ARE PERFORMED TO REFRACTURE THE SOIL PROFILE THROUGH THE 12-IN COMPACTION ZONE. SUBSTITUTE METHODS MUST BE APPROVED BY THE ENGINEER. ROTOILLERS TYPICALLY DO NOT TILL DEEP ENOUGH TO REDUCE THE EFFECTS OF COMPACTION FROM HEAVY EQUIPMENT. DO NOT COMPACT BIORETENTION SOIL WITH MECHANICAL EQUIPMENT.

EMBANKMENT/BERM FILL

A. CONSTRUCT EMBANKMENT/BERM IN ACCORDANCE WITH SPECIFICATIONS AND AS INDICATED ON DRAWINGS.

INSTALLATION

- A. DO NOT CONSTRUCT THE BIORETENTION AREA UNTIL ALL DISTURBED AREAS WITHIN THE
- CONTRIBUTING DRAINAGE AREAS HAVE BEEN GRADED AND STABILIZED. REMOVE SEDIMENT ACCUMULATED ALONG THE EXCAVATION FLOOR DURING SITE CONSTRUCTION PRIOR TO CONTINUING WITH THE BIORETENTION FACILITY CONSTRUCTION.
- FORM BOTTOM OF EXCAVATION TO CORRECT ELEVATION.
- D. IF INFILTRATION IS PROMOTED, THEN RIP THE BOTTOM SOILS TO A DEPTH OF SIX INCHES TO PROMOTE GREATER INFILTRATION.
- E. INSTALL THE FILTER FABRIC ALONG THE EXCAVATION SIDE WALLS AS SPECIFIED IN THE DRAWINGS. IF FILTER FABRIC IS TO BE INSTALLED PLACE THE FILTER FABRIC ON THE SIDES OF THE BIORETENTION AREA WITH A MINIMUM SIX INCH OVERLAP AT ALL JOINTS.
- INSTALL ANY TEMPORARY EROSION AND SEDIMENT CONTROLS TO DIVERT STORMWATER AWAY FROM THE
- G. BIORETENTION AREA DURING FINAL CONSTRUCTION AND UNTIL IT IS COMPLETED. SPECIAL PROTECTION
- MEASURES SUCH AS EROSION CONTROL FABRICS MAY BE NEEDED TO PROTECT VULNERABLE SIDE
- SLOPES FROM EROSION DURING THE CONSTRUCTION PROCESS.
- ESTABLISH ELEVATIONS AND PIPE INVERTS FOR INLETS AND OUTLETS AS INDICATED ON DRAWINGS INSTALL THE OVERFLOW OUTLET STRUCTURE AS INDICATED ON DRAWINGS.
- INSTALL UNDERDRAIN, INCLUDING 1.5" PERFORATED PIPE, GRAVEL AND FILTER FABRIC ON TOP OF THE UNDERDRAIN GRAVEL AS INDICATED ON DRAWINGS. PLACE GRAVEL AROUND THE UNDERDRAIN PIPE AS INDICATED IN THE DETAILS. OBSERVATION WELLS AND/OR CLEAN-OUT PIPES MUST BE PROVIDED. M. INSTALL PEA GRAVEL LAYER AS INDICTED ON DRAWINGS.
- N. DELIVER APPROVED BIORETENTION SOIL AND STORE ON ADJACENT IMPERVIOUS AREA OR PLASTIC SHEETING.

BACKFILLING

- A. BACKFILL WITH APPROVED BIORETENTION SOIL TO THE DESIGN GRADE AS SPECIFIED IN THE DRAWINGS
- B. PLACE SOIL IN 12 INCH LIFTS UNTIL DESIRED TOP ELEVATION OF BIORETENTION SOIL IS ACHIEVED. DO NOT USE HEAVY EQUIPMENT WITHIN THE BIORETENTION BASIN. HEAVY EQUIPMENT CAN BE USED AROUND THE PERIMETER OF THE BASIN TO SUPPLY SOILS AND SAND. WAIT 3 DAYS TO CHECK FOR SETTLEMENT, AND ADD ADDITIONAL MEDIA AS NEEDED
- C. DO NOT COMPACT BIORETENTION SOIL WITH MECHANICAL EQUIPMENT.
- D. GRADE BIORETENTION MATERIALS WITH LIGHT EQUIPMENT SUCH AS A COMPACT LOADER OR A DOZER/LOADER WITH MARSH TRACKS.

E. STABILIZE ALL REMAINING DISTURBED AREAS AND SIDE SLOPES WITH SEEDING, HYDROSEEDING, AND/OR EROSION CONTROL BLANKETS AS INDICATED ON DRAWINGS.

8. PLANTING

- A. PLANT BIORETENTION AREA IN ACCORDANCE WITH PLANTING PLANS AND SPECIFICATIONS. B. THE PRIMARY FUNCTION OF THE BIORETENTION STRUCTURE IS TO IMPROVE WATER QUALITY. DO NOT ADD FERTILIZERS OR OTHER SOIL AMENDMENTS TO THE BIORETENTION SOILS UNLESS INSTRUCTED BY THE ENGINEER. THE PLANTING SOIL SPECIFICATIONS PROVIDE ENOUGH ORGANIC MATERIAL TO ADEQUATELY SUPPLY NUTRIENTS FROM NATURAL CYCLING.
- C. INSTALL BIORETENTION PLANTINGS AS INDICATED ON DRAWINGS AND WATER AS NOTED ON DRAWINGS AND IN SPECS.
- D. DO NOT PLANT BEFORE THE REMAINING DISTURBED AREAS SURROUNDING THE FACILITY ARE STABILIZED.
- REMOVE SEDIMENT ACCUMULATED IN THE BIORETENTION AREA DURING THE PLANTING PHASE IF SUITABLE VEGETATIVE COVER HAS NOT BEEN ESTABLISHED ALONG THE BIORETENTION SIDE SLOPES PRIOR TO PLANTING, INSTALL A SILT FENCE PERIMETER AT THE TOE OF THE BIORETENTION SLOPES AND LEAVE IN PLACE UNTIL AN APPROVED VEGETATIVE COVER HAS BEEN ESTABLISHED.
- G. REMOVE REMAINING EROSION AND SEDIMENT CONTROLS ONLY AFTER SURROUNDING DISTURBED AREAS HAVE BEEN PROPERLY STABILIZED.
- H. CONDUCT FINAL CONSTRUCTION INSPECTION WITH ENGINEER

9. CLEAN UF

A. AFTER COMPLETION OF THE WORK, REMOVE AND PROPERLY DISPOSE ALL DEBRIS, CONSTRUCTION MATERIALS, RUBBISH, EXCESS SOIL, ETC., FROM THE PROJECT SITE. REPAIR PROMPTLY ANY IDENTIFIED DEFICIENCIES AND LEAVE THE PROJECT SITE IN A CLEAN AND SATISFACTORY CONDITION

CONSTRUCTION SEQUENCE:

THE FOLLOWING CONSTRUCTION SEQUENCE IS TO BE USED AS A GENERAL GUIDELINE. COORDINATE WITH THE OWNER, ENGINEERS, AND LANDSCAPE AND APPROVAL PRIOR TO CONSTRUCTION.

- 1. CONDUCT A PRE-CONSTRUCTION MEETING.

- **BIORETENTION CONSTRUCTION.**
- STABILIZED.
- STORMWATER AWAY FROM THE BIORETENTION AREA.
- SUBDRAIN SYSTEM.
- FIELD VISIT AND REPORT REQUIRED SEE NOTE (3) BELOW.
- INFILTRATION
- 12. BELOW.
- IMPERVIOUS AREA OR PLASTIC SHEETING.
- BACKFILL WITH APPROVED BIORETENTION SOIL TO THE DESIGN GRADE SUBMIT A SOIL SAMPLE (1 GALLON) TO THE ENGINEER PRIOR TO SOIL
- BELOW
- FACILITY ARE STABILIZED.
- FIELD VISIT AND REPORT REQUIRED SEE NOTE (3) BELOW.
- REMOVE REMAINING EROSION AND SEDIMENT CONTROLS ONLY AFTER
- 20. SEE GENERAL CONSTRUCTION NOTES FOR OVERALL CONSTRUCTION SEQUENCE.
- DETAILED CONSTRUCTION REQUIREMENTS.
- 22. MANDATORY NOTIFICATION/APPROVAL OF THE PROJECT ENGINEER IS PROCEEDING DAY TO ARRANGE FOR ANY REQUESTED FIELD VISITS.



BIORETENTION SOIL MEDIA (BSM):

and Sealed For Construction.

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CKI	RR	RR				
DESCRIPTION	35% REVIEW	95% REVIEW				
DATE	4/9/17	6/4/17				
NO	-	7				
	WATERSTONE)	9 GRETA'S WAY	SIKATHAM, NH 03885 (p) 603.686.2488	
95% DESIGN FOR WATER INTEGRATION FOR SOUDMSCOTT -		EXELER (WISE) IN LEGRALED PLAN (IP) PHASE 1		LINCOLN SIREEL SUBWALERSHED	NI ITRIENT CONTROL STRATEGIES	
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	THE JETVAC IS TO BE SENT DOWN THE ENTIRE LENGTH OF THE SEPARATOR ROW. AS THE HIGH PRESSURE WATER NOZZLE IS RETRIEVED, THE CAPTURED SEDIMENTS ARE PUSHED BACK INTO THE MANHOLE FOR VACUUMING.	
	MAINTENANCE OF THE SEPARATOR ROW IS TO BE ACCOMPLISHED WITH A JETVAC PROCESS.	
	ACCESS WILL BE PROVIDED VIA A MANHOLE(S) LOCATED AT THE END(S) OF THE ROW FOR CLEAN OUT.	
	WHILE CLEANING IS POSSIBLE FROM A SINGLE MANHOLE IN SHORTER LINES, A CLEAN-OUT OPTION FROM EITHER END OF A LINE IS PREFERABLE, PARTICULARLY FOR LONGER RUNS. CLEANING INVOLVES FLUSHING SEDIMENT FROM THE BASE FABRIC OF THE SEPARATOR ROW.	
	CULTED RECOMMENDS INSPECTIONS OF THE SEPARATOR ROW TO BE PERFORMED EVERY SIX MONTHS FOR THE FIRST YEAR. THE FREQUENCY OF INSPECTION CAN THEN BE ADJUSTED BASED UPON PREVIOUS OBSERVATION OF SEDIMENT DEPOSITION.	
	THE SAME AS CULTEC'S REQUIREMENT DETAILED IN THE COMPANY'S INSTALLATION GUIDELINES WITH THE EXCEPTION OF THE PLACEMENT OF THE REQUIRED FILTERING FABRICS. PLEASE REFER TO CULTEC'S CURRENT INSTALLATION INSTRUCTIONS FOR STORMWATER CHAMBERS AS A GUIDE.	PIPE SIZE = 24.(
	SCOUKING OF THE STONE BASE DURING HIGH PRESSURE JETTING. THE RECOMMENDED INSTALLATION OF SEPARATOR ROW CHAMBERS, IN REGARD TO STONE SEPARATION AND STONE ABOVE THE UNIT, ALONG WITH OTHER MINIMUM BURIAL, MATERIALS AND METHOD SPECIFICATIONS DETAILED FOR THE PROPER INSTALLATION. IS	INSERTED A 8.0" [20 INTO STRUCTURE AN mm] MIN. INTO CHAM
	ONCE WRAPPED, THE SEPARATOR ROW IS TO THEN PLACED ENTIRELY OVER 2 LAYERS OF CULTEC NO. 66 WOVEN GEOTEXTILE. THIS WOVEN GEOTEXTILE PROVIDES A DURABLE SURFACE WITHIN THE ROW FOR MAINTENANCE PROCEDURES AS WELL AS TO PREVENT ANY	PIPE DESIGN AND E
	THE CHAMBERS UTILIZED IN THE SEPARATOR ROW ARE TO BE COMPLETELY WRAPPED WITH CULTEC NO. 410 NON-WOVEN GEOTEXTILE. THIS CREATES A PASS-THROUGH FILTER ARRANGEMENT TO SEPARATE TOTAL SUSPENDED SOLIDS IN THE TRANSFER OF STORM WATER TO OTHER CHAMBERS THROUGHOUT THE UNDERGROUND STORMWATER MANAGEMENT SYSTEM.	, FL
	FEED SYSTEM THAT DIVERTS THE FLOW OF CLEAN WATER TO THE OTHER PARTS OF THE UNDERGROUND STORMWATER MANAGEMENT SYSTEM. THE DISTRIBUTION SYSTEM MAY BE BY PIPES SET AT A LOWER ELEVATION THAT PERMIT THE FIRST FLUSH TO THE SEPARATOR ROW VERSUS OTHER PARTS OF THE UNDERGROUND STORMWATER SYSTEM. THIS INITIAL FLOW MAY BE MANAGED BY A BAFFLE OR WEIR. THE SIZING OF THE PIPE(S) THAT PROVIDE STORM WATER TO THE SEPARATOR ROW IS TO BE DETERMINED BY THE DESIGN ENGINEER AND IS BASED UPON THE REQUIREMENT TO ACCOMMODATE THE DESIGN FLOW AND SERVICE CONVENIENCE.	
	ROW IS THE SAME CHAMBER USED THROUGHOUT THE ENTIRE CHAMBER BED. STORMWATER IS DISTRIBUTED TO THE SEPARATOR ROW BY A PRIMARY FEED SYSTEM THAT DIVERTS FLOW TO THE SEPARATOR ROW AND A SECONDARY BYPASS	(330XLHD) 1.0
	A SEPARATOR ROW IS INSTALLED ON A 1-2 INCH [25-51 mm] WASHED, CRUSHED STONE BASE. TYPICALLY, THE CULTEC CHAMBER MODEL USED FOR THE SEPARATOR	14. THE GEOTEX
	EASIER AUGESS FOR INSPECTION AND MAINTENANCE.	METHOD.
	CULTEC'S SEPARATOR ROW IS USED AS AN INEXPENSIVE MEANS OF REMOVING TOTAL SUSPENDED SOLIDS FROM THE CHAMBER SYSTEM, AS WELL AS PROVIDING	13. THE GEOTEX
	GENERAL	11. THE GEOTEX
	SEPARATOR ROW™ SPECIFICATIONS	
(GENERAL NOTES	9. THE GEOTEX
		8. THE GEOTEX
		7. THE GEOTEX
	24. THE CHAMBER SHALL BE MANUFACTURED IN AN ISO 9001:2008 CERTIFIED FACILITY. 25. MAXIMUM ALLOWED COVER OVER TOP OF UNIT SHALL BE 12 FEET (3.66 m) 26. THE CHAMBER SHALL BE DESIGNED TO WITHSTAND TRAFFIC LOADS WHEN INSTALLED ACCORDING TO CUILTED'S RECOMMENDED INSTALLATION INSTRUCTIONS	6. THE GEOTEX
	INSPECTION PORT OR CLEAN-OUT. 23. THE UNITS MAY BE TRIMMED TO CUSTOM LENGTHS BY CUTTING BACK TO ANY CORRUGATION. 24. THE CHAMPER SHALL BE MANUEACTURED IN AN USO 2024 2029 CERTIFIED FACILITY.	5. THE GEOTEX
	21. HEAVY DUTY UNITS ARE DESIGNATED BY A COLORED STRIPE FORMED INTO THE PART ALONG THE LENGTH OF THE CHAMBER. 22. THE CHAMBER SHALL HAVE A 6 INCH (152 mm) DIAMETER RAISED INTEGRAL CAP AT THE TOP OF THE ARCH IN THE CENTER OF EACH UNIT TO BE USED AS AN OPTIONAL	3. THE GEOTEX
	END WALLS. THE UNIT SHALL FIT INTO THE SIDE PORTALS OF THE RECHARGER 330XLHD AND ACT AS CROSS FEED CONNECTIONS. 20. CHAMBERS MUST HAVE HORIZONTAL STIFFENING FLEX REDUCTION STEPS BETWEEN THE RIBS.	2. THE GEOTEX
	18. THE RECHARGER 330XLEHD END UNIT MUST BE FORMED AS A WHOLE CHAMBER HAVING ONE FULLY FORMED INTEGRAL ENDWALL AND ONE FULLY OPEN END WALL AND HAVING NO SEPARATE END PLATES OR END WALLS.	1. THE GEOTEX
	ENDWALL AND ONE PARTIALLY FORMED INTEGRAL ENDWALL WITH A LOWER TRANSFER OPENING OF 14 INCHES (356 mm) HIGH X 34.5 INCHES (876 mm) WIDE.	GEOTEXTILE PARA
	IN LEGRAL ENDWALL AND ONE PARTIALLY FORMED IN LEGRAL ENDWALL WITH A LOWER TRANSFER OPENING OF 14 INCHES (356 mm) HIGH X 34.5 INCHES (876 mm) WIDE. 17. THE RECHARGER 330XLIHD INTERMEDIATE UNIT MUST BE FORMED AS A WHOLE CHAMBER HAVING ONE FULLY OPEN	CULTEC NO. 66™ WOVE CAUSED BY WATER MC
	SEPARATE END PLATES OR SEPARATE END WALLS. 16. THE RECHARGER 330XLSHD STARTER UNIT MUST BE FORMED AS A WHOLE CHAMBER HAVING ONE FULLY FORMED INTEGRAL ENDWALL AND ONE PARTIALLY FORMED INTEGRAL ENDWALL WITH A LOWER TRANSFER OPENING OF 14	GENERAL
	SEPARATE END PLATES CANNOT BE USED WITH THIS UNIT. 15. THE RECHARGER 330XLRHD STAND ALONE UNIT MUST BE FORMED AS A WHOLE CHAMBER HAVING TWO FULLY FORMED INTEGRAL ENDWALLS AND HAVING NO	CULTEC NO. 66™
	13. THE RECHARGER 330XLHD CHAMBER SHALL HAVE 16 CORRUGATIONS. 14. THE ENDWALL OF THE CHAMBER, WHEN PRESENT, SHALL BE AN INTEGRAL PART OF THE CONTINUOUSLY FORMED UNIT.	INSTRUCTIONS.
	STONE. 12. THE RECHARGER 330XLHD CHAMBER SHALL HAVE FIFTY-SIX DISCHARGE HOLES BORED INTO THE SIDEWALLS OF THE UNIT'S CORE TO PROMOTE LATERAL CONVEXANCE OF WATER	9. THE CHAMBER SHAL
	10. THE NOMINAL STORAGE VOLUME OF THE RECHARGER 330XLHD CHAMBER SHALL BE 7.459 FT³ / FT (0.693 m³ / m) - WITHOUT STONE. THE NOMINAL STORAGE VOLUME OF A JOINED RECHARGER 330XLHD SHALL BE 52.213 FT³ / UNIT (1.478 m³ / UNIT) - WITHOUT STONE. 11. THE NOMINAL STORAGE VOLUME OF THE HVLV FC-24 FEED CONNECTOR SHALL BE 0.913 FT³ / FT (0.085 m³ / m) - WITHOUT	8. THE HVLV FC-24 FEE SEPARATE END WALLS CONNECTIONS CRFAT
	9. THE NOMINAL CHAMBER DIMENSIONS OF THE CULTEC HVLV FC-24 FEED CONNECTOR SHALL BE 12 INCHES (305 mm) TALL, 16 INCHES (406 mm) WIDE AND 24.2 INCHES (614 mm) LONG.	7. THE HVLV FC-24 FEE
	INTERNAL MANIFOLD. THE NOMINAL DIMENSIONS OF EACH SIDE PORTAL SHALL BE 10.5 INCHES (267 mm) HIGH BY 11.5 INCHES (292 mm) WIDE. MAXIMUM ALLOWABLE OUTER DIAMETER (O.D.) PIPE SIZE IN THE SIDE PORTAL IS 11.75 INCHES (298 mm).	6. THE NOMINAL STOR
	INCHES (1321 mm) WIDE AND 8.5 FEET (2.59 m) LONG. THE INSTALLED LENGTH OF A JOINED RECHARGER 330XLHD SHALL BE 7 FEET (2.13 m). 7. MAXIMUM INLET OPENING ON THE CHAMBER ENDWALL IS 24 INCHES (600 mm). 8. THE CHAMBER SHALL HAVE TWO SIDE PORTALS TO ACCEPT CULTED HVLV® EC-24 FEED CONNECTORS TO CREATE AN.	5. THE NOMINAL CHAM INCHES (614 mm) LONG

ALL ELECTRIC, GAS, TEL. WATER, SEWER AND DRAIN SERVICES ARE SHOWN IN SCHEMATIC FASHION, THEIR LOCATIONS ARE NOT PRECISE OR NECESSARILY ACCURATE. NO WORK WHATSOEVER SHALL BE UNDERTAKEN ON THIS SITE USING THIS PLAN TO LOCATE THE ABOVE SERVICES. CONSULT WITH THE PROPER AUTHORITIES CONCERNED WITH THE SUBJECT SERVICE LOCATIONS FOR INFORMATION REGARDING SUCH. CALL DIG-SAFE AT 811

CULTEC RECHARGER® 330XLHD PRODUCT SPECIFICATIONS

RECHARGING, DETENTION OR CONTROLLING THE FLOW OF ON-SITE STORMWATER RUNOFF

1. THE CHAMBERS SHALL BE MANUFACTURED BY CULTEC, INC. OF BROOKFIELD, CT, USA. (203-775-4416 OR 1-800-428-5832)

2. THE CHAMBER SHALL BE VACUUM THERMOFORMED OF BLACK HIGH MOLECULAR WEIGHT HIGH DENSITY POLYETHYLENE (HMWHDPE).

CULTEC RECHARGER 330XLHD CHAMBERS ARE DESIGNED FOR UNDERGROUND STORMWATER MANAGEMENT. THE CHAMBERS MAY BE USED FOR RETENTION.

5. THE CHAMBER SHALL BE JOINED USING AN INTERLOCKING OVERLAPPING RIB METHOD. CONNECTIONS MUST BE FULLY SHOULDERED OVERLAPPING RIBS, HAVING NO

GENERAL

CHAMBER PARAMETERS

THE CHAMBER SHALL BE ARCHED IN SHAPE.

4. THE CHAMBER SHALL BE OPEN-BOTTOMED.

GENERAL

CHAMBERS.

AGE VOLUME OF THE HVLV FC-24 FEED CONNECTOR SHALL BE 0.913 FT³ / FT (0.085 m³ / m) - WITHOUT STONE.

ED CONNECTOR MUST BE FORMED AS A WHOLE CHAMBER HAVING TWO OPEN END WALLS AND HAVING NO SEPARATE END PLATES OR S. THE UNIT SHALL FIT INTO THE SIDE PORTALS OF THE CULTEC RECHARGER STORMWATER CHAMBER AND ACT AS CROSS FEED ING AN INTERNAL MANIFOLD.

LL BE DESIGNED TO WITHSTAND TRAFFIC LOADS WHEN INSTALLED ACCORDING TO CULTEC'S RECOMMENDED INSTALLATION

EN GEOTEXTILE IS UTILIZED AS AN UNDERLAYMENT TO PREVENT SCOURING



